

MUNSON TWP.
M. Berry Co. 1875 Recd.

96

FIELD BOOK

307 T

PLEASE RETURN TO
GEAUGA COUNTY ENGINEER
COURT HOUSE
CHARDON, O.
PHONE 250- X

Mulberry Road - No. 39 - Sec. H

Align. - pg. 2-9

X-Sections - pg. 10-26

Slope Stakes - pg. 28-48

Grades - pg. 55-57

Mulberry Rd #39 Sec. H (1955) pg. 60

(96)

1
B. M. #13, Wilson Mills Road Survey
Nail in N.W. Corner Top Concrete Step.
Frame School House, "Bloody Corners."
El. 1253.965

Mulberry Road, from
W. Line of Munson Easterly to Meccasin Falls.

10+00 0°00' Hill Top

5+00 0°00'

P.T. 2+11.25 13°00'

2+00 12°16'

1+50 9°01'

P.L. 1+13.00 $\Delta = 26°00'R.$

1+00 5°46' $D = 13°00'$ $L = 200.00'$

0+750 2°31' $T = 101.75$ $E = 11.8$

P.C. 0+11.25

0+00 Chester-Munson Township Line

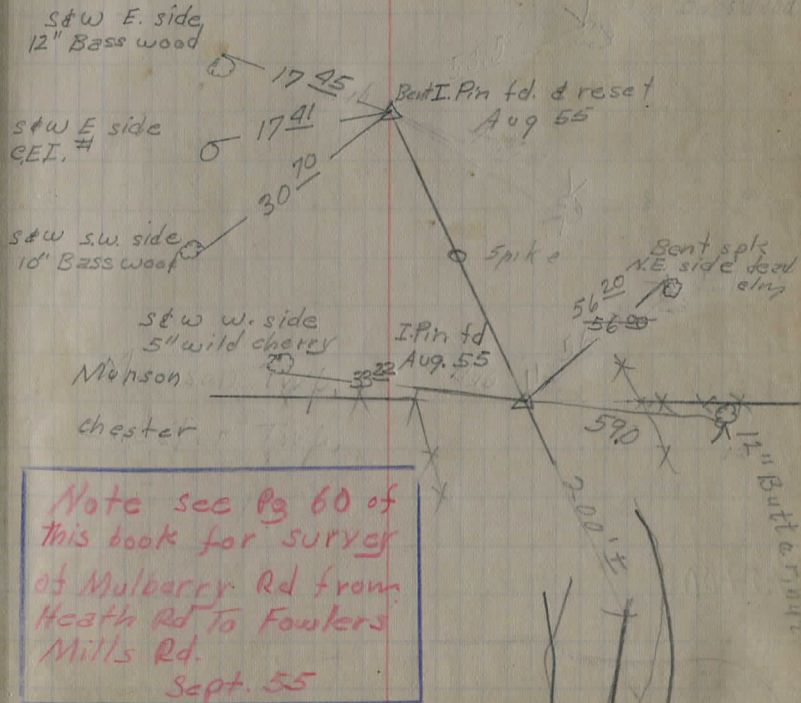
June 11, 1928, P.M.
Fair.

W.C. Marks, D. Parks
C. Rand, R. Hassel,

spike 25' stake

#. F. M. Mar
6+35

stake 0.25
10-27-30
D. Parks
F. Hassel
T. Snyder



31+00 A = 3°47' L, No Curve

30 0°00'

25+00 0°00'

23+50 0°00'

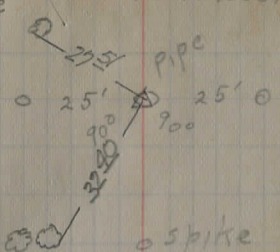
20+00 0°00'

15+00 0°00'

June 12, 1928 Marks - Parks
Fair, Warm
S&W w. side
10" Locust

I. Pipe fd
Aug. 55

S&W SW side
6" Basswood

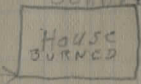


spike

spike

S&W S.W. side

24" Evergreen
John Vachal

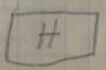


I. bolt fd.
Aug. 55

S&W N.W. side
12" Apple

Hub 25' stake

Grape Row stake 25' Hub.



55+00

0°00'

53+00

0°00'

Valley

50+00 $\Delta = 0^{\circ}29'$ Left, Summit

45+00

0°00'

40+00

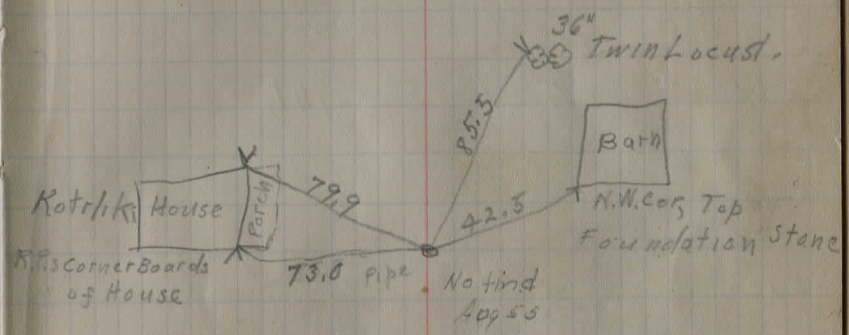
0°00'

3500

0°00'

stake 25' spike

spike 25' stake



spike 25' x stake

spike 25' x stake

spike 25' x stake

72+00

A = 1° 15' Right

70+00

0° 00'

65+00

0° 00'

60+00

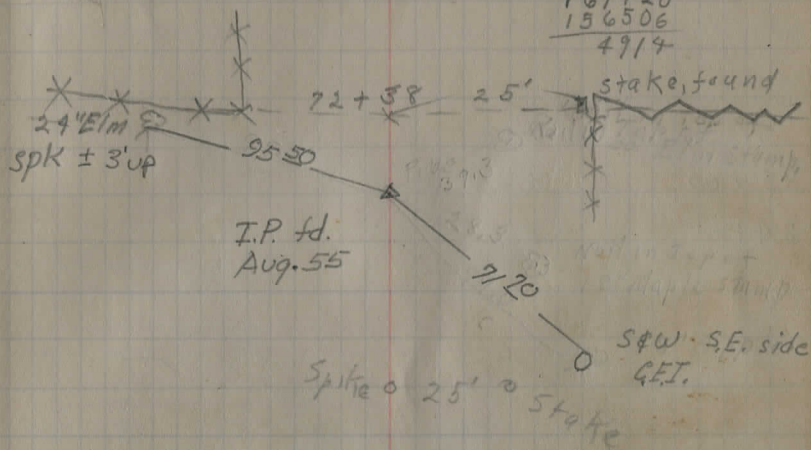
0° 00'

58+00

0° 00'

0.17
3.
1.51

2235.8) 7235.8
 5000.00
 2235.80
 3.85000 (00172
 22358
 161420
 156506
 4914



I.P. fd.
Aug. 55

Spike o 25' Stake
S.W. S.E. side
G.E.I.

Spike o 25' Stake

Spike
25' Stake

Stake
25' Spike - Driveway into Field

90+00 0°00'

85+00 0°00'

84+00 0°00'

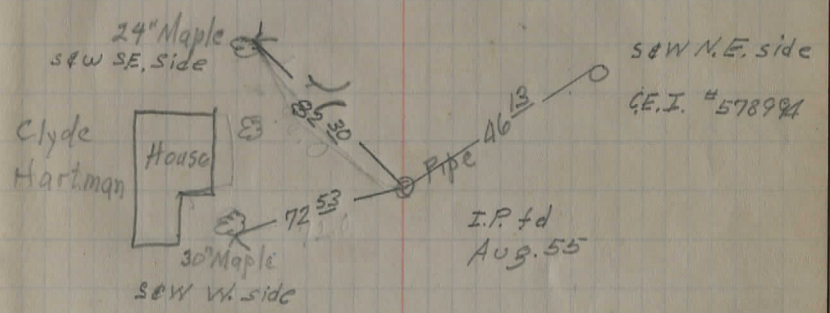
81+00 $\Delta = 1^{\circ}58'$ Right

80+00 $\Delta = 0^{\circ}00'$

75+00 0°00'

spike 25' stake

Staked 25' spike
Stake 25' spike



Staked 25' spike
79+11

P. Roseum
~~_____~~
C. Hill

stake 25' spike

93+80 P.T.

93+00 - 5°00'

93+40.07 P.I.

$\Delta = 8^{\circ}00' R.$

$D = 10^{\circ}$

$L = 80.0'$

$T = 40.07$

$E = 1.4'$

93+00 P.C.

98+00

97+00

0°00'

94+00

$\Delta = 3^{\circ}00' \text{ Right}$

93+00

$\Delta = 5^{\circ}00' \text{ Right}$

spk set
F.O.T. Sept. 2, 55



400.00 m

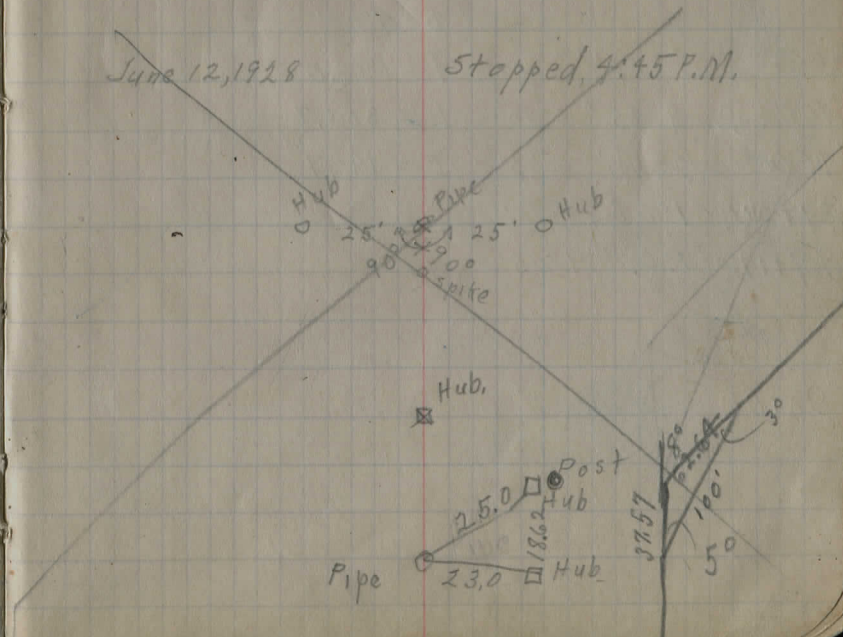


spk set
Sept. 2, 55

Started, Nov. 20, 1930

June 12, 1928

Stopped, 4:45 P.M.



102+27.3 P.T. $10^{\circ}47\frac{1}{2}'$

102 $9^{\circ}50'$

101+50 $8^{\circ}05'$

101 $6^{\circ}20'$

100+75 P.I. $\Delta = 21^{\circ}35'$ L.

D = 7000'

T = 156.0

L = 308.3

E = 14.7

100+50 $4^{\circ}35'$

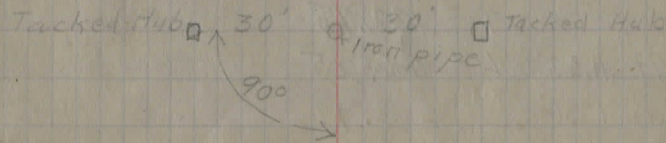
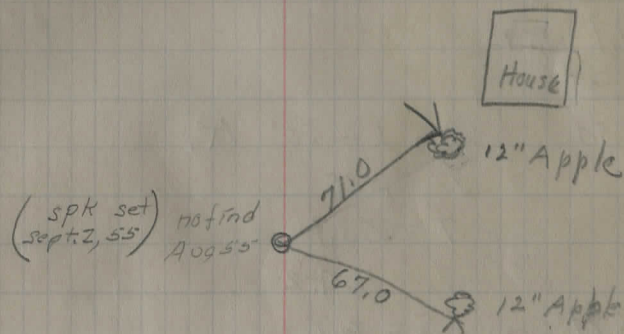
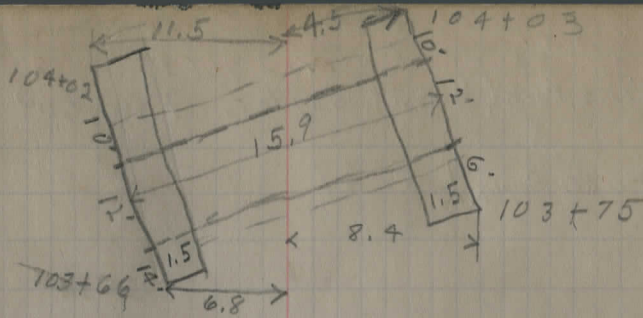
100 $2^{\circ}50'$

99+50 $1^{\circ}05'$

99+19.0 P.C.

98+00 $\Delta = 0^{\circ}00'$

Iron Pipe



Stopped, Nov, 20, 1930
Marks, Parks, Hassel, Snyder. Fair, 600

117+67.0 Approx. K. Road

115+11.1 P.T.

114+50 $\Delta = 24^{\circ} 50' R$,

$D = 20^{\circ}$

$T = 63.1$

$L = 124.2$

113+86.9 P.C. $E = 6.9$

110+85.1 P.T. 115.5'

P.T. 109+87.50

109+55 P.I. $A = 26^{\circ} 30' L$,

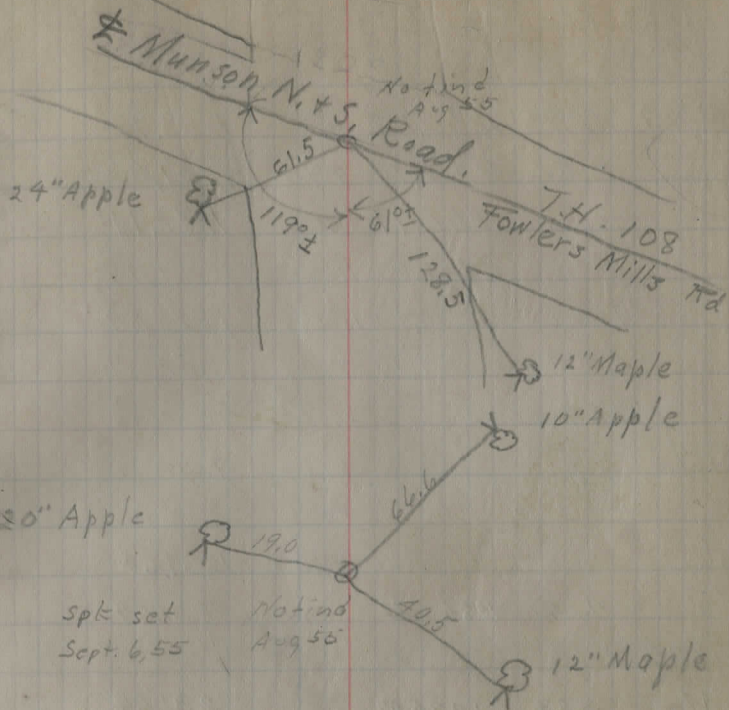
$D = 40^{\circ} 00'$

$T = 33.75$

P.C. 109+21.25 $L = 66.25$

108+50 P.O.T. $E = 3.9$

107+50 P.O.T.



spk set P.O.T.

(spk set Sept 3, 55)

No 1st Aug 55

194.32

25.5

12" Basswood

57.0

20" Maple

LEVELS
MULBERRY Road X SECTIONS

B.M. 13	2.25	1256.22	1253.97	
	2.52	1253.78	4.94	1251.26
	10.57	1052.77	11.64	1242.14
	0.58	1241.73	11.56	1241.15
	1.55	1230.44	12.84	1228.89
	4.73	1227.10	8.07	1222.37
	7.27	1231.71	2.66	1224.44
117+67.0		6.1		1225.6

B.M.		0.07	1231.64
	4.22	1235.86	1231.64
117+67.0			
B.M.	3.43	1235.07	1231.64

Broken in 5' from joint
10" vit pipe collect.

117+20	8.7	1226.4	1227.4
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117	8.3	1226.8	1227.8
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116	7.8	1227.3	1228.3
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115	7.9	1227.2	1228.2
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114+150	9.1	1226.0	
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	2.21	1229.65	7.63	1227.44
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114	4.9	1224.8	
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Nov. 21. 1930.
D. Parks, R. Mosel, T. Snyder
Fair 55°

Wilson Mills RD. Survey B.M. (now gone)
North W.W. corner Top conc. step Fr. Schmitt road

1231.3	North	1230.2	1228.1	1225.6	1221.8	1218.4	1217.2	1216.5	1214.4
0.4	1.5	3.6	6.1	8.9	13.3	14.5	15.2	15.3	12
150	100	50	4	50	100	150	200	250	300

S.W. root 12" Maple 150' N. of intersection

1234.0	1232.9	1232.4
1.9	3.0	3.5
300	250	300

9.1	8.0	9.4	9.9	9.0	8.7	8.7	9.7	11.5	12.0	13.9	17.2
30	30	25	14	14	13	12	10	12	25	50	118
Fence											
5.7	5.9	8.2	8.5	8.3	8.8	9.5	8.7	10.2	11.1		
30	18.5	13	10	2	7	15	10	25	30		

4.2	6.3	8.3	7.8	4.8	8.1	9.4	13.0	14.2
30	12	10	15	4	15	15	25	37

5.3	6.7	8.6	8.9	7.6	8.7	8.9	8.0	14.3
30	6	3	4	5	14	15	20	30

6.6	4.7	9.1	8.1	9.1	8.8	8.1
30	3	4	7	18.5	17.0	30

1.6	3.9	4.9	4.2	4.9	3.8	3.6	4.0
30	4	4	7.5	17	18	21	30

✓
1229.65

113 7.1 1222.6

112 10.4 1219.3

5.56 1222.43 12,78 1216.87

111 7.7 1214.7

110+70 10.7 1211.7

3.97 1214.22 12.18 1210.25

110 10.9 1203.3

10.19 1211.66 12.75 1201.47

109+55 14.6 1197.1

2.10 1200.84 12.92 1198.74

109+21.25 7.4 1193.4

B. M. 7.17 1193.67

109 9.8 1191.0

0.28 1189.19 11.93 1188.91

108 3.6 1185.6

107 10.6 1178.6

1.19 1178.03 12.35 1176.84

106 2.6 1175.4

105 4.7 1173.3

$\frac{4.8}{30} \frac{6.2}{6} \frac{8.0}{5} \frac{7.1}{4} \frac{6.7}{11} \frac{7.5}{15} \frac{6.4}{16.5} \frac{6.3}{20} \frac{6.9}{30}$

fence

$\frac{6.9}{30} \frac{8.6}{5} \frac{10.8}{2.5} \frac{10.4}{4} \frac{9.5}{7} \frac{10.3}{15} \frac{8.7}{17} \frac{8.9}{21} \frac{8.9}{30}$

fence

$\frac{3.0}{30} \frac{3.5}{16} \frac{4.5}{11.5} \frac{8.1}{6.5} \frac{7.8}{3} \frac{7.7}{4} \frac{7.5}{5} \frac{8.0}{13} \frac{8.9}{15} \frac{7.0}{17} \frac{8.5}{20} \frac{8.5}{30}$

fence

$\frac{4.1}{30} \frac{5.1}{18} \frac{12.9}{8} \frac{10.9}{3} \frac{10.7}{4} \frac{11.0}{12} \frac{11.6}{14} \frac{8.7}{19.5} \frac{8.9}{25} \frac{9.4}{30}$

$\frac{0.5}{30} \frac{0.5}{23} \frac{16.9}{6.5} \frac{10.9}{9.5} \frac{11.9}{4} \frac{11.0}{10} \frac{5.3}{17} \frac{8.1}{20} \frac{8.1}{30}$

fence

$\frac{0.0}{35} \frac{0.6}{30} \frac{4.1}{18.5} \frac{15.4}{7} \frac{14.6}{4} \frac{14.6}{4} \frac{14.4}{11} \frac{15.1}{13.1} \frac{9.9}{19} \frac{8.8}{23} \frac{9.2}{30}$

fence

$\frac{0.3}{30} \frac{2.3}{11} \frac{6.2}{5} \frac{8.1}{2} \frac{7.4}{4} \frac{6.8}{15.5} \frac{7.5}{17} \frac{6.2}{19} \frac{4.1}{25} \frac{7.3.3}{27} \frac{7.3.3}{30}$

fence

N.W. root 24" Maple 30 ft sta. 109+10

$\frac{6.6}{30} \frac{8.1}{18} \frac{7.7}{40.5} \frac{10.6}{7.5} \frac{9.8}{4} \frac{8.8}{1.5} \frac{8.5}{15} \frac{9.6}{18} \frac{8.4}{19.5} \frac{8.0}{25} \frac{8.8}{30}$

fence

$\frac{1.8}{30} \frac{1.3}{20} \frac{0.5}{15} \frac{2.3}{10} \frac{4.1}{9} \frac{4.7}{7.5} \frac{3.6}{4} \frac{3.6}{4} \frac{4.0}{10.5} \frac{4.4}{12} \frac{2.6}{14} \frac{2.3}{12.5} \frac{3.2}{20} \frac{3.2}{30}$

fence

$\frac{8.8}{30} \frac{10.3}{17} \frac{2.6}{14} \frac{12.6}{12.5} \frac{11.7}{11} \frac{10.6}{4} \frac{10.7}{4} \frac{11.5}{8} \frac{10.8}{9.5} \frac{10.1}{30}$

fence

$\frac{2.7}{30} \frac{2.3}{18} \frac{3.8}{15} \frac{2.6}{12} \frac{2.6}{4} \frac{2.7}{4.5} \frac{2.5}{6} \frac{2.4}{9.5} \frac{4.5}{13} \frac{4.5}{30}$

fence

$\frac{5.1}{30} \frac{4.7}{24.5} \frac{4.6}{15} \frac{5.8}{13} \frac{4.3}{7} \frac{4.7}{4} \frac{5.0}{6} \frac{2.2}{15} \frac{2.3}{12.5} \frac{0.8}{30}$

fence

✓
1178.63

104+75		5.2	1172.8
	3.02	1176.73	4.32 1173.71
104+30		4.8	1171.9
104		4.4	1172.3
103+88	Cone bridge	4.1	1172.6
B.M.		6.73	1171.00
B.M.		6.73	1170.00

4.0	5.7	5.4	4.6	5.3	5.2	5.5	0.1	4.4	4.5
30	24	15.5	15.10	8.5	4	4	14	22	30

5.8	4.9	5.9	4.7	4.8	7.0	6.0		
30	24	15	13	11	8	4	22	30

15.8	7.5	7.3	8.8	8.8	3.9	4.4	4.4	4.2	3.8	2.9	8.7	10.0
30	24	15	14	11.5	11.5	7.0	4	3.5	5.3	6.0	15	30

fence
 between W & N
 W side
 N side
 1167.80
 1165.2
 1165.2
 1171.7
 1173.6
 1172.7
 1172.6
 1172.7
 1173.7
 1171.7
 1165.3
 1169.8
 1169.2
 1162.0
 1161.0
 F.L.

N. E root 12" Maple 30' RT, sta. 103+40

Nov. 22, 1930
 D. Parks
 R. Hassel
 T. Snyder

Cold Wind 40°

N.E. root 12" Maple 30' Ft. Sta. 103+40

B.M	12.00	1182.00	1170.00
103		9.4	1172.6
102+273		5.2	1176.8
	11.64	1190.31	3.33 1178.67
102		10.4	1179.9
101+80		7.9	1182.4
101+50		6.1	1184.2
101		4.0	1186.3
101+50		1.4	1188.9
	13.01	1202.45	0.87 1189.44
100		9.8	1192.7
99+50		5.1	1197.4
	12.02	1214.45	0.02 1202.93
99		10.9	1203.6
	8.40	1221.85	1.00 1213.85
98		10.1	1211.8

14.0	11.5	9.4	9.1	9.9	10.6						
30-23	22	13	4	8	23	30					
In creek		Fence									
9.4	8.7	3.9	5.2	6.1	5.7	6.2	3.8				
30	16	4	4	2	3	19	30				
Fence											
18.5	17.5	8.8	10.4	16.1	10.7	11.6	11.3	9.7	7.6		
30	28	7	4	7	2	16	20	30	35		
Fence											
16.6	8.3	5.5	3.9	9.1	7.9	9.1	8.3	8.2	5.3	5.9	
35	27	20	17	12	7	4	18	18.5	21	25	30
Fence											
5.3	4.2	5.6	6.1	6.1				6.3	5.6		
30	16	14	2	1	4			18.5	30		
Fence											
6.5	5.8	4.1	7.0	4.2	3.9	6.4	7.2	4.7	4.7		
30	12	5	4	7.5	9	14	30				
Fence											
3.4	3.2	1.6	1.4	1.6	3.7	3.3	4.1				
30	17	16.5	7	4	7	10	30				
Fence											
11.9	11.8	10.0	9.6	9.8	10.0	11.4	9.2	9.9	9.8	9.5	
30	19	14	5	4	2	3	7	11	25	30	
Fence											
7.5	6.5	5.4	5.1	5.1	6.1	4.1	3.9	0.2			
30	21	14	4	3	4	7	16	30			
Fence											
5.4	8.3	12.1	14.6	10.9	11.2	12.0	7.9	4.4	3.9		
30	22	15	10	8.5	4	3.5	8	12	24	30	
Fence											
4.8	5.3	10.1	10.5	10.1	10.3	12.3	10.0	9.7	5.3		
30	17	10	4	4	11.5	16	18	20	25	30	
Fence											

1221.85

97+25 6.7 1215.2

97 6.1 1215.8

6.91 1222.10 6.64 1215.19

96 6.6 1215.5

95 7.6 1214.5

94+75 1 1/4" pipe 7.8 1214.3

94 6.5 1215.6

93 4.5 1217.6

92 4.3 1217.8

B.M 3.81 1218.29

91 5.4 1216.7

7.91 1223.12 6.89 1215.21

90+85 12" corr pipe 6.9 1216.2

90 5.7 1217.4

87+15

5.8 4.3 5.8 7.6 7.1 6.7 7.1 7.7 6.9 5.4
30 26 10 7 5 4 12 14 17 30

6.2 6.7 7.5 6.8 6.1 6.1 6.6 7.5 6.6 5.9
30 10 8 6.5 4 5 11 12 13 30

6.9 7.1 8.1 7.3 7.3 6.6 6.6 7.4 7.9 7.4 6.6
30 10 9 7 5 4 5 11 12 13 30

9.1 8.8 8.2 7.6 7.8 9.3 8.6 8.8
30 8 6 4 9 13 14 30
1213.8 1213.4 1212.4 1213.5 1214.1 1214.3 1213.9 1212.9 1212.3 1211.9 1210.8 1209.9
8.3 8.7 9.7 8.6 8.1 8.8 8.2 9.2 9.8 10.2 11.3 12.2
100 50 2.5 6.5 6.5 4 8 8.5 8.5 15 50 100
12.2 10 6 4 7.0 5.4 10.8 5.4 13.2 15.0 1208.9 1208.4 1207.9

5.9 6.9 7.3 6.5 6.8 7.4 6.3 6.1
30 13 11 4 4 7 9 30

4.3 4.6 4.9 7.5 5.2 7.8 5.1
30 10 9 4 8 9 30

4.1 4.8 5.3 4.3 4.9 4.9 4.0
30 11 11 8.5 4 7 30

N. root 24" Evergreen 30' RT. Sta. 91+75

5.3 5.6 5.7 5.6 6.1 6.9
30 5 4 8 10 30
1217.2 1216.3 1213.1 1213.9 1215.1 1216.4 1216.2 1216.0 1214.0 1213.1 1212.0 1208.3 1205.4
5.9 6.3 10.0 9.2 8.1 6.7 6.9 7.1 8.1 10.0 11.1 11.8 12.7
100 75 10.5 10.5 10.5 7 4 6 10 11 11 50 100
7.4 7.4 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00

4.5 5.0 6.8 5.7 5.7 6.1 6.5 5.8 5.3
30 14 11 9 4 7.5 6.5 8 30

✓
1223,12

89+15 15" vit pipe 4.9 1218.2

89 4.7 1218.4

9.61 1229,29 3.44 1219.68

88+70 10.4 1218.9

88+60 9.7 1219.6

88 8.7 1220.6

87 5.7 1223.6

86 3.0 1226.3

12.23 1241.32 0.20 1229.09

85 11.3 1230.0

84 7.8 1233.5

83 2.5 1238.8

12.80 1254.09 0.03 1241.29

12.03 1261.86 4.26 1249.83

82 13.3 1248.6

F.M 0.04 1261.82

1216.8
1216.3
1214.4
1215.6
1217.1
1217.8
1218.2
1218.2
1218.2
1214.3
1213.2
1207.15
1201.15

6.3 6.8 8.7 7.5 6.1 5.3 4.9 4.9 8.8 9.9 10.4 16.0 22.0
100 50 13.5 13.5 16.5 7.5 2 2.5 10 11 11 30 100
FL 7.00
Sun. Dumped out lot
1218.2
7.49 P.L.

5.8 5.7 5.2 4.2 4.7 4.7 9.7 10.5 10.5
30 20 18 11 2 17 19 30

9.8 10.3 10.8 10.0 10.4 11.1 10.5
30 18 15 5 2 11 30

7.0 8.2 10.1 9.8 10.6 9.7 10.5 8.9 9.1
30 25 21 16 13.5 11.5 11 18 30

4.6 8.5 9.6 8.7 8.7 9.0 9.7 6.8 7.3
35 21.17 15.11 2 4 6 10 30

4.5 4.5 6.8 6.0 5.7 6.1 6.9 5.4 6.4
30 20 15.5 13 2 4 7 10 30

2.2 1.7 3.7 2.8 3.0 3.2 3.5 2.5 3.8
30 18 17 13.5 2 5 15 9 30

11.1 11.1 12.8 12.2 11.3 11.9 12.7 11.3 12.9
30 16 15 12.5 2 6 8 10 30

5.9 7.3 9.5 8.1 7.8 8.1 9.3 7.8 8.5
30 18 15 13.5 2 5.5 7 11 30

0.4 1.5 4.0 2.7 2.5 2.8 1.3 0.8 0.5
30 17 15.5 13.5 2 5 8 10 30

7.0 8.3 11.6 14.2 13.7 13.3 13.1 13.8 7.2 8.0
30 20 17 12 10.5 2 7 9 19.5 30

S.W. root 30" Maple 70 lt. sta. 81+40.

✓
126186

81 4.9 1257.0

80 0.9 1261.0

✓
10.85 1272.02 0.69 1261.17

79 8.7 1263.3

78 6.2 1265.8

77 2.4 1269.6

T.P. 2.33 1269.69

$\frac{1.7}{30}$ $\frac{3.2}{15}$ $\frac{6.8}{10}$ $\frac{5.1}{8}$ $\frac{4.9}{4}$ $\frac{5.4}{10}$ $\frac{5.9}{12}$ $\frac{3.0}{17}$ $\frac{3.1}{30}$

$\frac{1.03}{30}$ $\frac{0.0}{17}$ $\frac{2.5}{15}$ $\frac{1.7}{11}$ $\frac{0.9}{4}$ $\frac{1.2}{9.5}$ $\frac{1.3}{6.5}$ $\frac{0.7}{8}$ $\frac{2.7}{30}$

$\frac{9.8}{30}$ $\frac{8.7}{20}$ $\frac{8.7}{17}$ $\frac{9.5}{15}$ $\frac{8.8}{13.5}$ $\frac{8.7}{4}$ $\frac{8.8}{4}$ $\frac{12.2}{30}$

$\frac{3.4}{30}$ $\frac{4.7}{19}$ $\frac{5.9}{16}$ $\frac{6.9}{13}$ $\frac{6.2}{4}$ $\frac{6.5}{5}$ $\frac{7.1}{7}$ $\frac{6.4}{9}$ $\frac{7.2}{30}$

$\frac{11.1}{30}$ $\frac{10.8}{15}$ $\frac{3.3}{12.5}$ $\frac{2.9}{11}$ $\frac{2.4}{4}$ $\frac{3.0}{6}$ $\frac{3.9}{9}$ $\frac{1.3}{11}$ $\frac{1.0}{25}$ $\frac{1.0}{30}$

⊙ on large rock 15' N + sta 77+30

D. Parks
R. Haussel
T. Snyder

Showers + snow in afternoon

2 on large rock 15' Rt, sta. 77+30

T.P. 12.63 1282.32 1269.69

76 7.4 1274.9

10.32 1290.80 1.84 1280.48

75 11.4 1279.4

74 5.5 1285.3

8.07 1298.48 0.39 1290.41

73 8.1 1290.4

72 4.8 1293.7

71 3.8 1294.7

70 4.6 1293.9

69+80 culvert 4.8 1293.7

67 4.8 1293.7

3.81 1298.00 4.29 1294.19

68 4.4 1293.6

67 4.3 1293.7

B.M. 3.15 1294.85

5.6 6.4 8.0 7.8 7.4 7.6 7.9 7.1 8.4
30 16 14.5 13 4 5 7.5 9 30

Fence
6.5 8.0 12.4 11.7 11.4 11.7 12.2 9.2 9.5
30 18.5 14.5 12 4 4 5.5 9 30

2.1 6.9 6.4 5.7 5.1 5.5 6.2 4.1 4.2
30 24 14.5 11.5 4 4 6 7 30

5.0 6.7 9.7 8.1 9.1 6.8 7.5
30 23 19 13 4 8 10 30

Fence
3.9 4.5 5.8 5.4 4.8 5.3 6.1 5.1 5.5 4.8
30 11 9 8.5 7 8.5 12 13 18.5 30

2.6 3.7 5.2 4.4 3.8 4.2 5.6 4.5 4.8
30 25 9 7 6 4 11 13.5 15 27 30

3.9 3.9 4.8 6.1 5.5 4.6 4.3 5.1 5.8 5.2 6.1
30 15 8.5 7 6 4 3.5 11.5 13.5 15 28 30

1283.2 1286.4 1289.9 1291.5 1292.0 1292.8 1293.3 1293.7 1293.4 1292.8 1292.3 1292.3 1293.7 1294.2
15.3 15.1 8.6 20 6.5 5.7 5.2 4.8 5.1 5.7 6.2 6.2 4.8 4.3
150 100 30 25 13 13 12 4 2.5 3 3 8 8.5 30
F.L. T.H.R.

3.6 3.6 4.4 5.7 5.1 4.8 5.2 6.5 5.0 4.9
30 25 8 4 4 4 14 16 17 28.5 30

4.9 4.8 5.7 4.9 4.9 3.8 4.7 5.7 4.7 4.7 4.1
30 24 8 6.5 5 4 6.5 13.5 16 17 20 29 30

5.5 4.8 5.6 4.8 4.3 3.9 4.4 5.1 4.4 3.8
30 25 9 5 4 4 6 14 15 16 30

Two spikes
A N. root 24" Ash 27' Rt. Sta. 66+98

1298.00

66		3.4	1294.4
65		4.9	1293.1
64		8.5	1289.5
63		12.1	1285.9
	1.24	1286.86	12.38 1285.62
62		6.0	1280.9
61		12.9	1274.0
	0.01	1274.93	11.94 1274.92
60		8.0	1266.9
B.M		3.54	1271.39
59		13.4	1261.5
	0.96	1262.98	12.91 1262.02
58		8.0	1255.0
	5.21	1255.48	12.71 1250.27
57		8.9	1246.6
	2.72	1245.38	12.82 1242.66
56		10.7	1234.6
	3.87	1236.47	11.78 1232.60
55		14.9	1221.6

3.6 30	3.6 24	3.7 6	4.9 5	4.1 3	3.6 £	3.1 4	3.6 15	4.5 16.5	3.0 19	2.7 30	
Fence grapes											
5.0 30	4.7 7	5.9 5	4.9 4	4.4 5	5.1 14	5.4 15	4.0 18	3.0 30			
8.8 30	8.6 7	9.8 5.5	9.3 4.5	8.5 £	8.1 5	8.3 12.5	9.8 15.5	7.3 19	5.8 30		
12.3 30	12.7 7	13.1 5.5	12.7 4	12.1 £		11.9 13.5	12.2 16	10.4 20	8.8 30		
4.6 30	5.5 8.5	7.6 6.5	6.9 5	6.0 £		6.4 11	6.8 13.5	4.7 15	2.6 30		
Fence											
9.6 30	10.7 13.5	14.6 10	13.9 9	12.9 £	13.4 8	14.2 10	14.6 13.5	10.1 18	9.2 20	7.9 30	
7.3 30	6.9 25	7.5 16	9.7 14	8.4 12	8.0 £	8.5 7	9.2 8	7.3 11	4.8 15	3.7 30	
Pett spike											
N. E. root 36" Maple 20' Rt. Sta. 60+05											
12.3 30	12.0 27	12.3 17	14.7 16-15	14.2 14	13.0 4	13.4 £	13.6 7	14.7 8	13.1 9	10.9 16	10.4 30
4.8 30	5.2 22	8.8 14.7	7.8 15	5.1 7.5	8.0 £	8.0 1	8.3 6	5.9 7	4.2 18	3.4 30	
2.5 30	3.5 20	10.1 15	9.4 7.3	8.9 £	8.9 3.5	10.2 7.5	4.5 10-18	2.6 22	2.4 30		
2.5 30	4.4 19	9.2 14	11.4 13	10.6 11	10.7 £	11.0 5	11.8 8-10	5.5 15	4.8 14.5	2.9 21	0.6 30
6.2 30	6.2 25	7.5 20	16.6 13	15.2 10	14.9 £	14.9 5	15.8 7-10	7.6 17	2.2 30		
Fence											

1236.47

54 1.26 1225.46 12.27 1224.20

54 0.20 1212.71 12.95 1212.51
3.6 1209.1

53 1.83 1202.29 12.25 1200.46
2.6 1199.7

52 5.2 1197.1

51+90 5.0 1197.3

B.M. 10.96 1213.17 0.08 1202.21
10.47 1202.68

51 10.7 1202.5

544 1218.43 0.18 1212.99

50 4.0 1212.4

49 11.3 1207.1

P.P. 12.98 1205.45

10.6 11.6 11.6 12.9 14.4
30 27 23 15 20 30

Fence

57 4.3 3.6 4.2 5.4 3.9
17-10 9 8 12 16.5

4.0 3.7 2.8 3.3 2.7 2.6 3.1 4.1 3.5 3.2 1.0
30 23 17 13 11 7 6 10 13.5 21 30

Fence

7.8 7.5 7.7 5.2 5.2 5.3 8.6 8.9 10.3
30 17 16 9 4 6 13 25 30

1191.8 1191.8 1192.1 1192.0 1193.2 1197.1 1197.3 1196.8 1192.0 1191.2 1191.0 1189.7 1188.8
105 105 102 10.3 9.1 5.2 5.0 5.5 14.3 14.1 11.3 12.6 13.5
118 50 118 115 11.5 7.5 4 7.5 7 9 25 25 25 100 100
118 10.6 F.L. T.O.P. T.O.P. F.L. 15.0 16.4 118.9
251 210 750 200

N. foot 30" locust 27' ft. sta 51+00

6.6 8.6 11.2 10.7 11.4 12.2 10.4 10.9 11.5
30 12 8 4 7 10 13 25 30

2.6 4.8 6.1 6.8 4.5 4.9 4.3
30 13 9 4 10 13.5 30

8.8 10.0 12.3 11.0 11.3 11.4 12.1 10.1 8.9
30 18.5 14 5 4 3.5 6 9 30

N. side Tel. pole Rt. sta 48+60

D. Parks
H. Barton
S. Meritt

cloudy
Cold. 28°

N. side tel. pole Rt. sta. 48+60

T.P.	0,37	1205,82	1205,45
48		6.7	1199.1
47		16.7	1089.1
	0.20	1193.71	1193.57
46+55		9.0	1184.8
	1.40	1182.40	1181.00
46		5.9	1176.5
	0.88	1170.26	1169.38
45		3.3	1167.0
44		11.5	1158.8
	0.34	1158.40	1158.06
43+45		3.8	1154.6
43		8.4	1150.0
42+70		11.2	1147.2
42-160		12.5	1145.9
	1.39	1146.72	1145.33
42		7.0	1139.7
	1.58	1135.42	1134.04
41		6.3	1129.3

Reverse this section

36	4.9	4.1	7.2	6.7	6.7	7.1	4.6	3.2	3.3
30	27	18	76	14	4	6	10	25	30
12.4	12.3	12.3	17.0	16.7	16.7	17.9	14.8	13.2	14.1
30	18	14	12.5	4	3	5	8	19	30
3.9	5.0	9.9	9.4	0.0	9.1	9.9	7.7	6.0	6.3
30	18	73	11.5	4	4	6	8	12.5	30
0.7	0.4	1.8	2.9	6.2	6.0	5.9	5.7	6.1	2.4
30	25	22	72.5	3.5	7.5	4	5.5	7	10.5
1.3	2.0	2.2	5.1	4.1	3.3	3.4	4.0	1.6	0.8
20	19.5	17	15	11.5	9.5	4	7	7	12
21	21	21	30	21	30	12	21	30	1.5
6.1	12.1	12.8	13.4	11.5	11.8	12.6	10.9	11.8	12.9
23	19	17.5	13.5	12	11	4	5	8	10
1.3	4.8	5.1	3.9	3.8	3.8	4.9	2.4	5.5	
30	16.5	13.5	11	4	5	7	9.5	30	
1.9	3.3	2.1	8.5	8.4	8.5	9.1	5.6	8.2	
30	19	12.5	11	4	5	7	9	30	
8.9	7.7	11.9	11.5	11.2	11.5	12.3	4.1	9.5	
30	11	6	4	4	11.5	13.5	22	30	
4.6	5.3	13.6	13.1	12.5	12.4	12.8	12.1	11.6	11.8
30	23.5	13.5	11	4	6	8	9	16	30
0.7	0.9	7.8	7.1	7.0	7.4	4.3	3.0	2.6	
30	27.5	15.5	11	5	4	13.5	3.0	2	
2.6	4.7	7.1	6.8	6.3	6.0	7.3	4.9	3.0	4.4
30	23	16.5	14.5	13	4	5	8	10.5	21

4045C
21.25
30
10W

1091.59 ✓

33 5.9 1085.7

32 4.1 1087.5

2.03 1089.64 ✓ 3.98 1087.61 ✓

31. 4.2 1085.4

30+35 12" cast iron pipe 4.7 1084.9

30 4.6 1085.0

B.M. 6.04 1083.60 ✓

4.6	4.1	4.9	5.2	7.3	6.4	5.9	6.7	7.1	4.9	3.8	2.1	6.5	6.5	
30	25	21	18	14	13	11	4	5	6	8.5	15	21	25	30

fence
row

3.9	6.9	5.2	5.7	5.0	4.1	4.5	5.7	4.5	2.3	2.4
30	21.5	12.5	12	10	4	5	9	9	24	30

fence
row

11.7	16.2	8.6	7.1	4.8	4.2	4.4	5.6	4.7	4.5	1.4	0.9	0.5
35	30	20	13	6	4	7.5	9.5	11	16	20	25	30

fence
row

18.5	14.5	9.2	8.4	7.3	5.2	4.7	5.0	6.1	6.6	5.4	3.1	1.6	1.5
30	24	14	F.L.	11	8	4	5	8	8	11	16	22	30

1071.1 1075.1 1080.4 1081.2 1082.3 1084.4 1084.9 1084.6 1083.5 1083.0 1084.2 1085.1 1084.0 1084.1

fence
row

8.3	5.9	5.1	4.6	4.8	5.8	4.5	1.3	1.1	1.0	
30	19	11.5	4	3	5.5	6.5	7.5	19	25	30

fence
row

gant spruce. Left
S. root 30" Maple 25 At? Sta, 29175

Dec. 22, 1930

23

D. Parks
H. Barton
S. Merritt

Cloudy cold 28°

B.M. 7.81 1091.41 1083.60

29 5.4 1086.0

28 5.2 1086.2

27 4.4 1087.0

8.40 1097.14 2.67 1088.74

26 9.0 1088.1

25 6.9 1090.2

5.10 1101.19 1.05 1096.09

24 6.4 1094.8

23+65 4.8 1096.4

23 5.3 1095.9

22 8.8 1092.4

0.54 1089.00 12.73 1088.46

21 3.8 1085.2

20 8.3 1080.7

B.M. 9.19 1079.81

Bent spike S. root 30" Maple 25' left sta. 29+75

8.8 7.9 6.1 6.6 5.2 5.2 5.4 5.7 6.6 5.1 5.2 3.2 2.4
30 22 15.5 13.5 12.5 7 4 2.5 4-5 6 11 17 20 30
1087.29.8 9.1 5.8 4.8 5.2 5.4 6.5 5.7 5.4 3.5 2.0
30 23 12 5.5 4 2 3 7 12 20 30
1087.28.7 5.4 5.7 5.0 4.3 4.4 4.7 5.1 4.9 4.7 3.0 2.6 2.1
30 15 13 11 5 4 2 4 5 11 20 20 30
1087.211.3 9.5 9.8 9.5 8.5 9.0 9.2 9.6 9.0 8.0 4.3 3.4
30 17 15.5 14 7 4 1.5 2.5 3.5 4 11 22 30
1087.26.1 5.6 4.9 6.6 6.1 6.9 7.2 5.8 2.1 0.8
30 17.5 16.5 13.5 7-4 4 2.5 3.5 7.3 30
1087.26.1 5.3 7.1 6.5 6.0 6.4 6.1 4.7 3.3 2.3
30 17 15 14 7 4 4 6 9 30
1087.25.7 4.9 6.1 5.4 4.4 4.8 5.0 3.5 2.7
30 17 15 13.5 8-6 4 2.5 3.5 5 30
1087.25.0 4.8 6.2 5.6 4.8 5.3 5.7 6.4 4.9 4.7 5.0
30 16 14 12 7-3 4 3.5 5 7 15 30
1087.26.0 7.0 9.8 9.3 8.8 9.7 10.2 7.5 6.9 7.8
30 13 10 8 4 7 8 10 14 30
1087.24.3 0.7 4.3 4.1 3.8 4.5 5.0 2.9 1.0 1.1
30 14 8 7 4 8 9 10.5 15.5 30
1087.26.1 8.1 9.6 8.8 8.3 8.9 9.6 8.7 10.8
30 9.5 7.5 5.5 7 8 10-11 11.5 30
1087.2

Bent spike

A.N. side 15" Walnut 25' Rt, sta. 20+15

✓
1089.00

19 10.9 1078.1
3.75 ✓ 1081.73 11.02 1077.98
12" CORR P. 12
18+45 Inlet of pipe 4.2 1077.5
Plugged Completely)

18 4.6 1077.1
2.43 ✓ 1079.80 4.36 1077.37

17 3.7 1076.1

16 7.5 1072.3

15 8.7 1071.1

14+70 11" Cast Iron pipe 8.6 1071.2

14+70 continued. on east side

14 8.8 1071.0

13 8.5 1071.3

12+50 ✓ 7.7 1072.1
11.53 ✓ 1084.39 6.94 1072.86

12 11.1 1073.3

11 6.2 1078.2

9.2 108 118 112 10.9 10.6 11.4 12.5 11.9 14.8
30 8.5 6 5 4 3 10 12.5 14 30
1080.8 1078.8 1077.5 1076.5 1075.0 1073.2 1071.5 1071.8 1071.2 1070.6 1070.1 1070.0 1070.0
09 29 4.2 5.2 4.7 4.5 4.2 3.2 4.5 4.9 5.2 6.0 6.3 7.4 8.0
30 30 8 6.5 5 2 4 3.5 11 11.5 12 12 20 30 75

2.3 4.1 5.5 4.9 4.6 4.3 5.1 5.2 5.4 7.2
30 7.5 6 7.5 4 7 11 12.5 13.5 30

10.8 0.2 1.3 4.7 4.1 3.7 3.2 3.8 4.8 3.3 3.7 4.1
30 20 10 5.5 3.5 4 5 11.5 13.5 15 25 30

3.5 5.5 6.9 8.2 7.7 7.5 7.3 8.3 9.8 12.1
30 20 8 6.5 4 4 3.5 14.5 14 30

5.6 8.7 9.6 8.8 8.7 8.7 9.4 10.9 12.8
30 7 7.6 4 4 4 10 16 30
1070.8 1070.5 1069.7 1069.5 1070.3 1070.9 1071.2 1071.3 1070.2 1069.7 1068.9 1068.2 1067.9
9.8 9.3 10.1 10.3 9.5 8.9 8.6 8.5 9.6 10.1 10.9 11.6 15.0
17 9 7.5 7.5 7.5 7.5 4 4 11.5 11.5 11.5 24 50

1075.3 1074.4 1073.3 1071.7 1071.1 7.0 0. Ground
7.5 5.4 6.5 8.1
30 34 29 28

from well
6.7 7.4 8.3 8.8 8.7 9.3 10.1 10.8
30 27 20 4 4 11 17 30

8.1 9.3 9.6 8.9 8.5 8.8 10.9 12.4
30 5.5 4 3 4 12 16 30

6.5 8.1 8.6 8.1 7.7 7.8 8.4 8.4 8.3
30 5.5 4 3 4 15 16 25 30

11.3 11.3 14.9 11.3 11.1 10.8 11.4 11.8 14.6 12.9
30 7 6 3 4 10 12.5 13.5 14.5 30

4.4 5.3 6.1 7.2 6.7 6.2 6.8 7.5 7.6 3.3 2.9 1.7
30 7 9 7.5 7 4 7.5 9 11 15 2.5 30

1084.39

B.M. 5.49 1088.61 1.27 1083.12
3.57 1085.04

10+50 5.9 1082.7

10 3.5 1085.1

9+45 5.4 1083.2

9 8.6 1080.0

8+40 12.1 1076.5

7 2.64 1078.88 12.37 1076.24

8 4.0 1074.9

7 6.1 1072.8

6+50 6.8 1072.1

B.M. 8.64 1070.24

6 9.3 1069.6

5+60 12.0 1066.9

N.W. root 30" Butternut, 30' Ft. Sta. 10+90

5.8 4.6 5.9 7.1 6.6 5.9 6.2 7.5 4.8 6.9 0.4
30 18 8 6.5 5 4 9 10 13 17 30
row

6.2 4.5 5.0 4.2 3.5 3.3 4.1 4.8 2.7 2.0 1.5
30 9 8 5 4 7.5 7.5 10-11 14 20 30
row

6.4 5.2 6.8 6.2 5.4 5.8 6.8 4.5 3.9 2.9 2.9
30 8 4.5 5 4 10 12 14 17 20 30
row

6.7 5.6 5.7 7.4 10.2 9.3 8.6 8.7 9.1 10.0 6.4 4.8 5.2
30 20.5 14 8 6 4 4 6 7 11.5 16 20 30
row

11.6 11.2 11.9 13.1 12.5 12.1 11.7 12.3 12.9 11.9 11.8 11.4 11.0
30 21 12 6-5 7 4 13-6 8 12 13 14 18 22 30
row

6.1 5.4 4.7 4.3 4.0 3.7 4.1 4.8 4.5 4.4 3.0
30 16.5 4 4 4 11 14 19.5 20 30
row

14.6 12.4 9.3 8.1 6.5 6.1 6.1 6.3 4.0 3.3 2.3
100 80 30 12 5.5 4 11 21 30 35 50
row

11.5 9.9 7.9 6.8
30 28 9 4
row
cart mark
tree

S.E. root 30" Walnut 28 left 6+40

12.8 10.0 9.6 10.0 9.3 9.6 8.2 7.4 6.7
30 14.5 10 8 4 8 9 10 30
row

14.1 10.9 11.0 13.2 12.9 12.0 11.8 13.7 9.0 8.2
30 19 10 9 6 4 6.5 11 15 25 30
row

✓
1078.88

5 ✓ 13.9 1065.0

0.95 1067.51 12.32 1066.56

4 ✓ 13.4 1054.1

0.20 1054.79 12.92 1054.59

3+25 Natural Drain S.W. For 4 1/2 ac. E. side 8.9 1045.9

3 ✓ 11.8 1043.0

0.26 1042.40 12.65 1042.14

2 8.2 1034.2

1+50 ✓ 12.6 1029.8

1.17 1030.98 12.59 1029.81

1 ✓ 7.0 1024.0

4.83 1023.21 12.60 1018.38

0+50 6.4 1016.8

0+00 11.9 1011.3

B.M. ✓ 7.75 1015.46

24 9.1 10.1 15.2 14.8 13.9 14.5 14.8 9.6 8.5 8.6
30 17 13 6 7.5 4 5 10 16 25 30

5.5 6.4 10.3 14.6 13.9 13.4 14.2 15.2 11.6 10.8 9.6 9.2
30 20 10.5 7 5 4 8 9.5 13 18 20 30

52.5 8.6 6.6 8.1 8.4 10.6 9.4 8.9 9.7 10.9 8.1 8.9 14.5 12.5
50.8 21 17 12 10.5 9.5 7.5 4 8 10 11 17 22 30 40

7.2 9.9 10.5 13.5 12.2 11.8 12.4 13.5 11.5 15.6 18.6
30 19 14 11 9 4 9.5 9.5 11-13 17 22 37

4.5 5.3 7.3 8.3 10.3 8.9 8.2 8.9 10.1 8.0 8.3 10.2 13.8
30 21 17 13 17-11 9 4 9 10-11 12 20 30 40

10.7 10.2 11.0 14.3 13.4 12.6 13.1 14.5 11.4 13.6 14.0
30 21 13 13-12 10 4 8.5 9.5 11-14 20 24 30

5.3 5.7 6.7 8.9 9.7 6.8 7.0 7.7 8.6 5.0 6.2 1.8 3.1
23 19 16 15 14 12 4.5 4 4.5 4 8 14 21 30

7.3 3.1 4.3 4.4 4.4 7.1 6.4 7.1 7.7 4.4 4.2 2.3
30 24 22 14 13-12 10 4 4.5 6-7 9 13 20 30

10.9 7.1 10.1 13.6 12.8 11.9 12.6 13.8 10.8 9.8 11.2
30 18 14.5 10.5 9 7.5 4 7.5 9-10 12 14 20 30

R. P. Spake E. side Elm Rt. sta. 0+45

Feb, 28, 1931

Slope stakes

21

Clear 40°

D. Parks
T. Snyder
S. Merritt

N. side E

S. side E

P.P. spike E, side Elm Pt. sta. 0+45

BM,	6.54	1022.00		1015.46
0+00				1014.50

7.50	7.64	$\frac{F0.1}{17.0}$	8.81	$\frac{F1.3}{19.0}$
------	------	---------------------	------	---------------------

0+50				1019.50
------	--	--	--	---------

2.50	2.80	$\frac{F0.3}{18.0}$	1.00	$\frac{C1.5}{22.0}$
------	------	---------------------	------	---------------------

	10.90	1032.64	0.26	1021.74
--	-------	---------	------	---------

8.64	6.25	$\frac{C2.4}{25.0}$	3.95	$\frac{C4.7}{22.0}$
------	------	---------------------	------	---------------------

1+00				1024.0
------	--	--	--	--------

3.14	0.38	$\frac{C2.7}{20.0}$	3.59	$\frac{F0.5}{23.0}$
------	------	---------------------	------	---------------------

1+50				1029.50
------	--	--	--	---------

	12.70	1043.50	1.84	1030.80
--	-------	---------	------	---------

9.00	6.58	$\frac{C2.4}{20.0}$	9.02	$\frac{0.0}{16.0}$
------	------	---------------------	------	--------------------

2+00				1034.50
------	--	--	--	---------

	12.55	1054.48	1.57	1041.93
--	-------	---------	------	---------

9.98	9.17	$\frac{C0.8}{20.0}$	12.55	$\frac{F2.6}{16.0}$
------	------	---------------------	-------	---------------------

3+00				1044.50
------	--	--	--	---------

	10.28	1064.71	1.05	1053.43
--	-------	---------	------	---------

10.21	3.12	$\frac{C7.1}{30.5}$	7.50	$\frac{C2.7}{23.5}$
-------	------	---------------------	------	---------------------

4+00				1054.50
------	--	--	--	---------

	10.76	1074.03	1.44	1063.27
--	-------	---------	------	---------

9.53	4.42	$\frac{C5.1}{26.5}$	3.73	$\frac{C5.8}{27.5}$
------	------	---------------------	------	---------------------

5+00				1064.50
------	--	--	--	---------

				1067.80
--	--	--	--	---------

6.23	7.01	$\frac{F0.8}{20.0}$	3.52	$\frac{C2.7}{22.0}$
------	------	---------------------	------	---------------------

5+60				1067.80
------	--	--	--	---------

				1070.00
--	--	--	--	---------

4.03	5.46	$\frac{F1.4}{17.5}$	1.92	$\frac{C2.1}{21.0}$
------	------	---------------------	------	---------------------

6+00				1070.00
------	--	--	--	---------

B.M.			3.89	1070.14 record
------	--	--	------	----------------

S.E. root 30" Walnut 28' left 6+40

	8.34	1078.58		1070.24 record
--	------	---------	--	----------------

6.58	8.09	$\frac{F1.5}{17.0}$	3.53	$\frac{03.1}{22.0}$
------	------	---------------------	------	---------------------

6+50				1072.00
------	--	--	--	---------

1078.58

7+00				1073.00
8+00				1075.00
8+40				1077.00
	12.70	1089.21	2.07	1076.51
9+00				1080.00
9+45				1082.50
10+00				1084.00
10+50				1082.00

B.M.		4.17		1085.04
	0.57	1085.61		1085.04 record
11				1079.50
12				1074.00
	3.27	1075.84	13.04	1072.57
12+50				1072.50
13				1071.30
14				1071.20

S. side

N. side

5.58	6.24	$\frac{F0.7}{18.5}$	7.92	$\frac{F2.3}{19.5}$
3.58	5.10	$\frac{F1.5}{15.5}$	4.02	$\frac{F0.4}{20.5}$
1.58	2.07	$\frac{F0.5}{19.5}$	1.00	$\frac{C0.6}{18.5}$
9.21	6.48	$\frac{C2.7}{24.0}$	5.26	$\frac{C4.0}{24.0}$
6.71	6.17	$\frac{C0.5}{20.0}$	3.18	$\frac{C3.5}{23.5}$
5.21	5.66	$\frac{F0.5}{19.0}$	2.40	$\frac{C2.8}{22.0}$
7.21	5.19	$\frac{C2.0}{21.5}$	1.21	$\frac{C6.0}{26.0}$

N.W. root 30" Butternut 30' Pt, sta. 10+90

6.11	5.99	$\frac{C0.1}{19.5}$	3.99	$\frac{C2.1}{22.0}$
11.61	12.05	$\frac{F0.4}{18.5}$	13.06	$\frac{F1.5}{17.5}$
3.34	3.30	$\frac{0.0}{19.5}$	4.35	$\frac{F1.0}{18.0}$
4.54	4.85	$\frac{F0.3}{19.0}$	6.67	$\frac{F2.1}{15.0}$
4.64	4.02	$\frac{C0.6}{19.5}$	5.93	$\frac{F1.3}{15.5}$

1075.84

1 9.46 1078.52 6.78 1069.06

15 1071.20 7.32 5.75

16 1073.00 5.52 3.74

9.56 1086.10 1.98 1076.54

17 1076.00 10.10 5.96

18 1077.50 8.60 7.67

19 1078.50 7.60 7.38

20 1081.00 5.10 4.05

B.M 6.13 1079.97

1079.81

check levels 1081.00

B.M 6.13 1085.94 1079.81

0.60 1076.98 9.56 1076.38

7.04 1075.94 8.08 1068.90

12.87 1085.29 3.52 1072.42

B.M. 0.40 1084.89

12.35 1092.16 1079.81

9.04 1100.37 0.83 1091.33

5.88 1093.94 12.31 1088.06

N side

S. side

$\frac{C1.6}{21.5}$

$\frac{F2.5}{18.0}$

$\frac{C1.8}{21.0}$

$\frac{F3.9}{21.0}$

$\frac{C4.1}{25.0}$

$\frac{C0.5}{19.5}$

$\frac{C0.9}{20.5}$

$\frac{F1.3}{16.0}$

$\frac{C0.3}{20.0}$

$\frac{F1.7}{17.0}$

$\frac{C1.1}{20.5}$

$\frac{F1.2}{17.5}$

Bent spike N. side 15" Walnut 25' Ft. 20+15

Bent spike N. side 15" Walnut 25' Ft. 20+15

N.W. root 30" Butterhut 30' Ft. sta. 10+90

Bent spike N. side 15" Walnut 25' Ft. sta. 20+15

1093.94

B. M.

10.48 1083.46

1083.60

Bent spike S. root 30" Maple 25' Left sta. 29+75

Mar. 6, 1931
Cold. Cloudy 30°
D. Parks
T. Snyder
S. Merritt. S. side &

N. side &

B. M. 12.53 1092.34 1079.81

Bent spike N side 15" Walnut 25' Ft. Sta. 20+15

21 1086.50 5.84 7.14 $\frac{C1.7}{21.0}$

2.46 $\frac{C3.4}{23.5}$

10.52 1101.06 1.80 1090.54

22 1092.50 8.56 7.61 $\frac{C1.0}{21.0}$

6.24 $\frac{C2.3}{22.0}$

23 1096.00 5.66 4.52 $\frac{C0.5}{19.5}$

4.93 $\frac{C0.1}{19.5}$

23+65 1096.50 9.56 2.56 $\frac{C2.0}{21.0}$

4.72 $\frac{F0.2}{17.5}$

24 1095.50 5.56 2.52 $\frac{C3.0}{23.0}$

5.27 $\frac{C0.3}{19.0}$

25 1091.50 9.56 5.19 $\frac{C4.9}{20.0}$

7.83 $\frac{F0.3}{23.0}$

5.63 1094.06 12.63 1088.43

26 1089.00 5.06 1.33 $\frac{C3.7}{23.0}$

6.87 $\frac{F1.8}{16.0}$

27 1087.00 7.46 5.58 $\frac{C1.5}{20.0}$

8.96 $\frac{F1.9}{17.0}$

28 1086.50 7.56 6.19 $\frac{C1.4}{19.5}$

9.92 $\frac{F2.4}{17.0}$

29 1086.00 8.06 5.77 $\frac{C2.3}{21.5}$

9.39 $\frac{F1.3}{17.5}$

B. M. 10.63 1083.43

Bent spike S. root 30" Maple 25' Left Sta. 29+75

10.38 1093.98 1083.60 record

30 1085.50 8.48 5.53 $\frac{C3.0}{22.5}$

10.22 $\frac{F1.7}{17.0}$

1093,98

31 1085,50

32 1085,50

3,47 1091,23 6,22 1087,76

33 1085,00

33+50 1083,75

33+80 1083,00

5,08 1085,62 10,69 1080,54

33+80 1083,00

34 1082,50

35 1083,00

12,77 1097,57 0,82 1084,80

36 1087,00

37 1093,00

13,06 1109,88 0,75 1094,82

37+85 1092,75

38 1101,20

13,09 1122,56 0,41 1109,47

39 1102,90

40 1119,60

S. side $\frac{1}{2}$

R

8,48 5,81 $\frac{C2,7}{18,0}$ 8,48 4,50 $\frac{C4,0}{24,0}$

slope hub Lt sta 33+00

8,23 2,09 $\frac{C4,1}{24,5}$ 7,48 2,53 $\frac{C5,0}{25,0}$

8,23

2,62 8,36 $\frac{F5,7}{25,0}$ 3,12 7,24 $\frac{F4,1}{24,5}$ 2,62 2,20 $\frac{C0,4}{19,5}$ 10,57 7,44 $\frac{C1,1}{19,0}$ 4,57 2,45 $\frac{C2,1}{21,0}$ 7,91 6,33 $\frac{C3,6}{23,5}$ 8,68 5,88 $\frac{C2,8}{22,0}$ 13,16 10,20 $\frac{C3,0}{22,0}$ 2,96 0,29 $\frac{C2,7}{22,0}$ N. side $\frac{1}{2}$

Lt

11,94 $\frac{F3,5}{22,5}$ 8,27 $\frac{F0,2}{19,0}$ 3,47 $\frac{C2,8}{21,5}$ 6,46 $\frac{C1,0}{18,0}$ 10,71 $\frac{F2,5}{18,0}$ 8,14 $\frac{F5,0}{17,0}$ 3,95 $\frac{F1,3}{18,0}$ 8,53 $\frac{C2,0}{21,5}$ 1,65 $\frac{C2,9}{23,0}$ 7,15 $\frac{C2,8}{22,5}$ 5,99 $\frac{C2,7}{23,0}$ 7,85 $\frac{C3,3}{22,5}$ 0,50 $\frac{C2,5}{22,0}$

1122.56

B.M., 11.46 1133.52 0.50 1122.06

B.M., 1.88 1131.64

13.09 1144.81 1131.72 record

41 1129.80

42 1140.00

12.99 1157.74 0.06 1144.75

42 1140.00

43 1150.00

43+45 1154.05

12.99 1162.67 1.06 1156.68

44 1159.00

45 1169.00

T.P., 0.24 1169.43

S. side £ N. side £

N. side Elm 25' Rt. sta. 40+85

N. root 86" Elm 25' Rt. sta. 40+85

15.01 11.23 $\frac{C 3.1}{22.5}$ 11.66 $\frac{C 3.4}{24.5}$

7.81 1.36 $\frac{C 3.5}{23.0}$

17.74 11.90 $\frac{C 5.8}{27.5}$

7.74 6.32 $\frac{C 1.4}{21.0}$ 1.72 $\frac{C 6.0}{27.0}$

3.69 3.17 $\frac{C 0.5}{19.5}$ 0.95 $\frac{C 2.7}{23.5}$

10.67 11.16 $\frac{F 0.5}{18.5}$ 10.06 $\frac{C 0.6}{19.5}$

0.67 0.24 $\frac{C 0.4}{19.0}$ 1.66 $\frac{F 1.0}{17.0}$

Slope hub Rt. sta. 45+00

	13.09	1182.52		1169.43
46				1179.00
	12.89	1194.85	0.56	1181.96
46+55				1184.50
47				1189.00
	12.86	1207.56	0.15	1194.70
48				1199.00
	10.40	1217.92	0.04	1207.52
49				1207.50
50				1210.50
	1.08	1206.31	12.69	1205.23
51				1204.50
B.M.		3.70	1202.61	1202.61
	3.70	1206.38		1202.68 record
52	12.30	1206.57	12.11	1194.27
52				1200.00
53				1202.00
	12.40	1218.52	0.45	1206.12
54				1210.50
	12.77	1230.73	0.56	1217.96
55	8.75	1237.48	2.00	1228.73
55				1222.50
56		7.16	1230.32	1222.50

Mar. 7, 1931
 Cold, Cloudy Snow 5:00 o'clock
 D. Parks, T. Snyder, S. Merritt

N. side $\frac{1}{2}$

slope hub Rt, sta. 45+00

S. side $\frac{C 2,3}{21.5}$ $\frac{1}{2}$

3.52	1.21	21.5	1.93	$\frac{C 1,6}{21.0}$
10.35	7.62	$\frac{C 2,7}{23.5}$	5.74	$\frac{C 4,6}{26.5}$
5.85	2.46	$\frac{C 3,4}{23.5}$	1.92	$\frac{C 3,9}{25.5}$
8.56	5.15	$\frac{C 3,4}{23.5}$	5.85	$\frac{C 2,7}{23.5}$
10.42	8.42	$\frac{C 2,0}{20.5}$	9.33	$\frac{C 1,1}{17.0}$
7.42	3.90	$\frac{C 3,6}{23.5}$	2.28	$\frac{C 5,1}{26.0}$
1.81	3.69	$\frac{F 1,9}{17.0}$	1.02	$\frac{C 0,8}{21.0}$
N. foot 30° Locust 27.78, sta. 51+00				
6.57	13.10	$\frac{F 6,5}{25.5}$	12.30	$\frac{F 5,7}{24.5}$
4.57	7.36	$\frac{F 2,8}{20.0}$	7.37	$\frac{F 2,8}{20.0}$
8.02	3.62	$\frac{C 4,4}{18.0}$	4.35	$\frac{C 3,7}{24.0}$
14.98	3.23	$\frac{C 11,8}{33.0}$	7.16	$\frac{C 7,8}{30.0}$
slope Hub Lt, sta. 55+00				

12,59 1242,91 1230,32

12,82 1255,55 0,18 1242,73

56 1234,50

57 1246,50

58 11,67 1266,90 0,32 1255,23

58 1255,00

59 1261,50

60 11,24 1277,35 0,79 1266,11

60 1268,00

B.M. 5,95 1271,40

5,95 1277,34 1271,39

61 12,89 1289,69 0,54 1276,80

61 1274,50

62 1281,00

12,70 1298,95 3,44 1286,25

63 1286,00

64 1290,00

65 1293,00

66 1294,00

B.M. 4,05 1294,90

1294,85

Mar. 17, 1931
Cloudy Cold 34°

D. Parks
T. Snyder

N. side &

S. side &

21,05 10,58 $\frac{C10,5}{33,0}$ 11,87 $\frac{C9,2}{31,0}$

9,05 2,20 $\frac{C6,9}{28,0}$ 1,47 $\frac{C7,6}{28,5}$

11,90 7,09 $\frac{C9,8}{24,0}$ 12,05 $\frac{F0,2}{19,0}$

5,40 2,42 $\frac{C3,0}{23,0}$ 3,90 $\frac{C1,5}{21,0}$

9,35 5,91 $\frac{C3,4}{22,5}$ 9,39 $\frac{0,0}{20,0}$

Bent spike N.E. ^{root} 30" Maple 20' Ft. Sta. 60+05

15,19 11,21 $\frac{C4,0}{23,5}$ 12,89 $\frac{C2,3}{22,5}$

8,69 5,59 $\frac{C3,1}{21,0}$ 7,67 $\frac{C1,0}{21,0}$

12,95 10,90 $\frac{C2,1}{18,5}$ 12,70 $\frac{C0,3}{18,5}$

8,95 8,44 $\frac{C0,5}{17,0}$ 9,26 $\frac{F0,3}{18,5}$

5,95 4,54 $\frac{C1,4}{18,5}$ 5,61 $\frac{C0,3}{19,5}$

4,95 3,65 $\frac{C1,3}{19,0}$ 4,64 $\frac{C0,3}{19,5}$

2 spikes N. root 24" Ash 27' Ft. Sta. 66+98

March, 23, 1931
Clear 45°
D. Parks
T. Snyder

N. side &

S. side &

B.M. 2.81 1297.66 1294.85

67 1294.00

68 1294.00

69 1294.00

5.11 1299.82 2.95 1294.71

70 1294.00

71 1294.00

72 1293.50

73 1290.40

74 1285.30

0.51 1288.24 12.09 1287.73

75 1280.20

3.07 1278.31 13.00 1275.24

76 1275.10

77 1270.00

78 1266.00

2 spike N. root 24" Ash 27' Pt. sta. 66+98

3.66 3.78 $\frac{F0.1}{18.0}$ 4.73 $\frac{F1.1}{17.5}$

3.66 4.14 $\frac{F0.5}{17.5}$ 4.41 $\frac{F0.8}{18.0}$

3.66 3.79 $\frac{F0.1}{17.5}$ 2.95 $\frac{C0.7}{20.0}$

5.82 6.38 $\frac{F0.4}{18.5}$ 5.49 $\frac{C0.3}{19.5}$

5.82 5.73 $\frac{C0.1}{19.0}$ 4.13 $\frac{C1.7}{21.0}$

6.32 6.59 $\frac{F0.3}{19.0}$ 5.36 $\frac{C1.0}{20.0}$

9.42 8.67 $\frac{C0.8}{20.5}$ 8.04 $\frac{C1.4}{17.0}$

14.52 13.16 $\frac{C1.4}{21.0}$ 12.09 $\frac{C2.4}{19.0}$

8.04 6.53 $\frac{C1.5}{20.5}$ 5.09 $\frac{C3.0}{22.5}$

3.21 3.66 $\frac{F0.5}{18.5}$ 2.05 $\frac{C1.2}{20.5}$

8.31 7.02 $\frac{C1.3}{20.0}$ 5.20 $\frac{C3.1}{24.0}$

12.31 12.87 $\frac{F0.4}{17.5}$ 11.08 $\frac{C1.2}{20.0}$

1278,31

1.56 1267,05 12,82 1265,49

79 1263,50

80 1261,00

81 1257,00

B.M 5,26 1261,79

5,26 1267,08 1261,82 record

3,30 1257,37 13,01 1254,07

82 1249,00

0,04 1244,89 12,52 1244,85

83 1240,50

84 1234,00

0,96 1232,75 13,10 1231,79

85 1230,00

86 1226,40

87 1223,40

88 1220,40

T.P. 9,86 1222,89

S. side 4

N. side 4

3,55 5,65 $\frac{F2,1}{17,0}$ 3,67 $\frac{F0,1}{18,0}$

6,05 6,76 $\frac{F0,7}{18,5}$ 4,29 $\frac{C1,8}{21,0}$

10,05 8,38 $\frac{C1,7}{21,8}$ 7,12 $\frac{C2,8}{23,0}$

S.W. root 30" Maple 70' Lt sta. 81+40

8,37 3,30 $\frac{C5,1}{26,5}$ 2,64 $\frac{C5,7}{27,0}$

4,39 4,66 $\frac{F0,3}{19,0}$ 4,09 $\frac{C0,3}{19,5}$

10,89 11,44 $\frac{F0,6}{18,0}$ 12,96 $\frac{F2,1}{15,0}$

2,75 2,95 $\frac{F0,2}{18,5}$ 2,48 $\frac{C0,3}{18,5}$

4,35 6,64 $\frac{F0,3}{19,0}$ 5,39 $\frac{C1,0}{18,5}$

9,35 9,42 $\frac{F0,1}{19,0}$ 8,23 $\frac{C1,1}{18,5}$

12,35 10,39 $\frac{C2,0}{18,0}$ 11,51 $\frac{C0,3}{20,0}$

Large stone Lt sta. 87+80

March, 24, 1931

Rain
D. Parks
F. Snyder

N. side ϵ

S. side ϵ

89 0.07 1222.96 1222.89 1218.40

90 1217.40

91 1217.00

4.70 1221.91 5.75 1217.21

B.M. 3.63 1218.28

3.63 1221.92 1218.29 record

4.56 13.02 $\frac{F8.5}{29.5}$ 5.41 $\frac{F0.9}{21.0}$

5.56 5.03 $\frac{C0.5}{19.0}$ 4.41 $\frac{C1.2}{23.0}$

5.96 6.38 $\frac{F0.4}{17.5}$ 7.73 $\frac{F1.8}{19.0}$

N. root 24' evergreen 30' Rt. sta. 91+75

~~92 1217.50~~

~~93 1217.50~~

~~94 1215.50~~

~~95 1214.50~~

~~6.01 1221.16 1221.15 6.77 1215.15~~

~~96 1215.20~~

~~97 1215.50~~

~~98 1211.00~~

~~0.29 1210.22 1210.21 11.23 1209.93 1209.92~~

~~99 1203.50~~

~~4.42 4.23 $\frac{C0.2}{19.0}$ 3.94 $\frac{C0.5}{19.5}$~~

~~4.42 4.54 $\frac{F0.1}{18.5}$ 4.10 $\frac{C0.3}{19.5}$~~

~~6.42 5.55 $\frac{C0.9}{20.0}$ 5.90 $\frac{C0.5}{20.0}$~~

~~7.42 8.73 $\frac{F1.3}{18.0}$ 8.77 $\frac{F1.4}{18.0}$~~

~~5.95 5.87 $\frac{C0.1}{18.5}$ 6.01 $\frac{F0.1}{19.0}$~~

~~5.65 5.35 $\frac{C0.3}{19.0}$ 5.25 $\frac{C0.4}{18.5}$~~

~~10.15 9.04 $\frac{C1.1}{18.0}$ 5.61 $\frac{C4.5}{28.0}$~~

~~6.71 0.29 $\frac{C6.4}{29.0}$ 2.83 $\frac{C3.9}{25.5}$~~

	1210,22 1210,21 1200,14 1200,13	1199,49 1199,48	
T.P. 99+50	0,65	10,73	1189,45
100			1195,00
	1189,28 2,23 1189,27	1187,05 1187,04	
100+50		13,09	1190,75
101			1186,50
101+50			1183,00
	1,34 1179,46	1178,12 1178,11	
102			1179,50
102+273			1178,00
103			1174,00
B.M.	10,35	1169,10 1170,00	
104			1172,00
105			1174,00

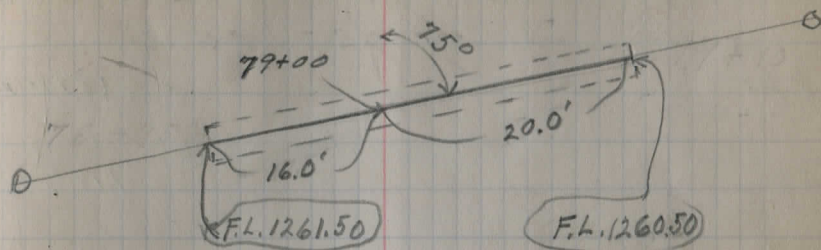
slope	stake	Ft.	sta.	99+50
0,88	0,65	$\frac{C 0,2}{20,0}$	4,27	$\frac{F 3,4}{19,5}$
5,13	8,43	$\frac{F 3,3}{18,0}$	10,46	$\frac{F 5,3}{22,5}$
+0,48	3,44	$\frac{F 3,9}{21,5}$	2,86	$\frac{F 3,3}{21,0}$
2,77	6,21	$\frac{F 3,4}{18,0}$	5,88	$\frac{F 3,1}{20,5}$
6,27	5,53	$\frac{C 0,7}{20,0}$	5,07	$\frac{C 1,2}{22,0}$
+0,05	1,34	$\frac{F 1,4}{18,0}$	7,50	$\frac{F 7,6}{28,0}$
1,45	4,19	$\frac{F 2,7}{17,5}$	7,55	$\frac{F 6,1}{24,0}$
5,45	7,94	$\frac{F 2,5}{16,5}$	8,97	$\frac{F 3,5}{18,0}$
N.E. root 12" Maple 30' Rt. sta. 103+40				

Mar. 30, 1931

Trustees authorized
Culvert across road
just above Clyde Hartman's House,
Marks recommended 36 ft. of 15" Pipe

B.M.
B.M 6.65 1268.47 1267.82
1261.89
1260.22

79+11 P. Roseum
C.Hill



S.W. root 30" Maple 70' Lt. sta. 81+40
6.58 4.58 C2.0 Stake, 30' Left
8.25 7.25 C1.0 Stake, 30' Right

106 1176.00

107 1179.00

108 1186.00

109 1195.00

B.M.
1193.67

N.W. root 24" Maple 30' Ft, Sta 109+10

B, M,	3.28	1221.57	1218.29
92			1217.50
93			1217.50
94			1215.50
95			1214.50
96			1215.20
97			1215.50
	3.06	1218.84	5.79 1215.78
98			1211.00
99			1203.50
	0.49	1206.83	12.50 1206.34
99+50			1199.25
	0.26	1194.63	12.46 1194.37
100			1195.00
100+50			1190.75
101			1186.50

No. root 24" evergreen 30' Ft, Sta, 91+75

4.07	3.89	$\frac{C0.2}{19.0}$	3.59	$\frac{C0.5}{19.5}$
4.07	4.20	$\frac{F0.1}{18.5}$	3.78	$\frac{C0.3}{19.5}$
6.07	5.24	$\frac{C0.8}{20.0}$	5.56	$\frac{C0.5}{20.0}$
7.07	8.37	$\frac{F1.3}{18.0}$	8.43	$\frac{F1.4}{18.0}$
6.37	6.32	$\frac{C0.1}{18.5}$	6.46	$\frac{F0.1}{19.0}$
6.07	5.79	$\frac{C0.3}{19.0}$	5.67	$\frac{C0.4}{18.5}$
7.84	6.78	$\frac{C1.1}{18.0}$	3.32	$\frac{C4.5}{28.0}$
15.34	8.97	$\frac{C6.9}{29.0}$	11.51	$\frac{C3.8}{25.5}$
7.58	7.44	$\frac{C0.1}{20.0}$	11.06	$\frac{F3.5}{19.0}$
+0.37	5.02	$\frac{F3.4}{18.0}$	5.04	$\frac{F5.4}{22.0}$
3.88	8.89	$\frac{F5.0}{21.0}$	8.31	$\frac{F4.4}{21.0}$
8.13	11.45	$\frac{F3.5}{21.0}$	11.30	$\frac{F3.2}{21.0}$

1194.63

101750

1188.00

0.13 1181.90 12.86 1181.77

102

1179.50

102+273

1178.00

103

B, M

12.51 1168.99

11.63

11.00

20.6

10.51

21.1

3.88

10.05

6.73

10.09

11.50

11.51

N.E. root 12" Maple 30' Ft. Sta. 103140

Mar, 31, 1931
D. Parks
T. Snyder
clear

April 1931
D. Parks
T. Snyder
Kaim

45

B, M.	12,92	1182,92		1170,00
103				1174,00
102+27,3				1178,00
102				1179,50
	12,55	1195,32	0,15	1182,177
101+50				1183,00
101				1186,50
100+50				1190,75
100				1195,00
	12,62	1207,35	0,59	1194,73
99+50				1199,25
	12,34	1219,34	0,35	1207,00
99				1203,50
98				1211,00
97				1215,50
	5,56	1222,29	2,61	1216,73

N. E. foot 12" Maple	30' Rt, Sta, 103+40			
2t	Rt			
8,92	11,57	$\frac{F2,6}{18,0}$	10,51	$\frac{F1,6}{16,0}$
4,92	10,10	$\frac{F5,2}{24,0}$	6,74	$\frac{F1,8}{17,5}$
3,42	10,07	$\frac{F6,7}{28,0}$	3,90	$\frac{F0,5}{18,0}$
12,32	10,20	$\frac{C2,1}{22,0}$	10,69	$\frac{C4,6}{20,0}$
8,82	11,01	$\frac{F2,2}{18,0}$	11,34	$\frac{F2,5}{18,0}$
4,57	8,00	$\frac{F3,4}{21,0}$	8,58	$\frac{F4,0}{21,5}$
0,32	4,74	$\frac{F4,4}{22,5}$	2,72	$\frac{F2,4}{18,0}$
8,10	10,58	$\frac{F2,5}{19,0}$	6,96	$\frac{C1,1}{20,0}$
15,84	11,07	$\frac{C4,8}{25,5}$	18,51	$\frac{C7,3}{29,0}$
8,34	2,85	$\frac{C5,5}{28,0}$	6,32	$\frac{C2,0}{18,0}$
3,84	2,48	$\frac{C1,4}{18,5}$	2,60	$\frac{C1,2}{19,0}$

1222,29

96	1215,20
95	1214,50
94	1215,30
93	1217,50
92	1218,50

B.M 3.02 1219,27
 1218,29 record

98
 97
 96
 95
 94
 93
 92

	Lt	Rt
	7.09	6.22
	<u>6.09</u>	<u>19.0</u>
	19.0	6.08
	<u>6.09</u>	<u>18.5</u>
	7.79	8.18
	<u>6.09</u>	<u>18.0</u>
	18.0	8.13
	<u>6.09</u>	<u>18.0</u>
	6.79	5.31
	<u>6.15</u>	<u>20.0</u>
	20.0	5.00
	<u>6.15</u>	<u>20.0</u>
	4.79	3.57
	<u>6.12</u>	<u>17.5</u>
	17.5	3.95
	<u>6.12</u>	<u>18.5</u>
	4.79	3.35
	<u>6.14</u>	<u>19.5</u>
	19.5	3.64
	<u>6.14</u>	<u>19.0</u>

N. foot 24" evergreen 30' Rt. sta. 91+75

<u>6.15</u>
28.0
<u>6.04</u>
18.5
<u>6.01</u>
19.0
<u>6.14</u>
18.0
<u>6.05</u>
20.0
<u>6.02</u>
19.5
<u>6.04</u>
19.5

<u>6.10</u>
18.0
<u>6.02</u>
19.0
<u>6.0</u>
18.5
<u>6.13</u>
18.0
<u>6.08</u>
20.0
<u>6.02</u>
18.5
<u>6.02</u>
19.0

April 4, 1931

47

D. Parks
T. Snyder
Clear 60°

B.M. 6.69 1176.69 1170.00

N.E. root 12" Maple 30' Rt. Sta. 103+40

104 1172.60

4.07 8.19 $\frac{F4.1}{14.5}$ 6.94 $\frac{E2.9}{6.5}$

104+75 1173.50

3.19 3.89 $\frac{F0.7}{17.0}$

104+75 10.97 1184.75 2.91 1173.78

104+75 1173.50

11.25 2.31 $\frac{C8.9}{31.5}$

105 1174.00

10.75 11.31 $\frac{F0.6}{18.5}$ 9.01 $\frac{C1.7}{21.0}$

106 1176.00

8.75 9.15 $\frac{F0.4}{17.0}$ 10.03 $\frac{F1.3}{18.0}$

107 1179.00

5.75 5.71 $\frac{0.0}{19.0}$ 5.21 $\frac{C0.5}{19.0}$

12.77 1197.34 0.18 1184.57

108 1186.00

11.34 9.54 $\frac{C1.8}{23.0}$ 10.54 $\frac{C0.8}{16.5}$

109 1195.00

2.34 5.22 $\frac{F2.9}{18.5}$ 4.68 $\frac{F2.3}{21.0}$

B.M. 3.68 1193.66

N.W. root. 24" Maple 30' Rt. Sta. 109+10

3.68 1197.35 1193.67 record

109+21.25 1197.12

0.22 2.22 $\frac{F2.0}{20.0}$

11.98 1208.74 0.59 1196.76

109+21.25 1197.12

11.62 10.37 $\frac{C1.3}{22.5}$

109+55 1200.50

8.24 7.16 $\frac{C1.1}{18.0}$

12.84 1221.40 0.18 1208.56

1221,40

109+55

1200,50

20,90

10,04

$\frac{C10,9}{35,5}$

110

1205,00

16,40

6,98

$\frac{C9,4}{33,0}$

11,98

$\frac{C4,4}{24,0}$

110+70

1211,30

10,10

2,80

$\frac{C7,3}{28,0}$

7,63

$\frac{C2,5}{22,0}$

111

1214,00

7,40

1,88

$\frac{C5,5}{27,0}$

6,01

$\frac{C1,4}{20,5}$

9,45 1230,51 0,34 1221,06

112

1219,50

11,01

7,77

$\frac{C3,2}{23,0}$

9,14

$\frac{C1,9}{21,0}$

113

1223,00

7,51

5,88

$\frac{C1,6}{21,0}$

6,85

$\frac{C0,7}{18,0}$

114

1226,00

4,51

2,91

$\frac{C1,6}{21,0}$

stake in traveled Roadway

114+50

1227,25

3,26

1,89

$\frac{C1,4}{20,0}$

115

~~1227,5~~
1228,50

3,01
~~2,01~~

1,13

$\frac{C1,9}{20,0}$
~~20,0~~
21,5

9,33

F0,3
 $\frac{F1,3}{17,5}$

7,97 1235,20 3,28 1227,23

116

1227,3
1228,30

7,90
6,90

5,24

$\frac{C2,7}{22,5}$
~~22,5~~

9,93

F2,0
 $\frac{F3,0}{16,0}$

117

1226,8
1227,80

8,40
7,40

5,61

$\frac{C2,8}{23,0}$
~~23,0~~

8,72

F0,3
 $\frac{F1,3}{14,5}$

B. M.

3,47 1231,73
1231,64

S. W. foot 12" Maple 150' N. of intersection

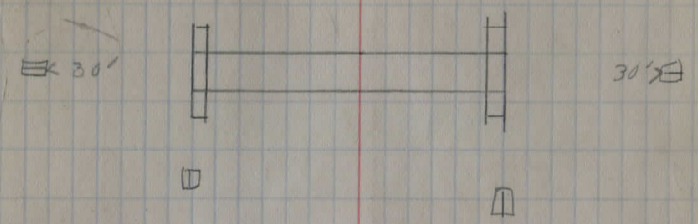
T.P. 8.09 1091.69 1083.60
 4.66 1085.42 10.93 1080.76

34
 34+00

7.92 C 5.0 1072.50
 10.92 1072.50

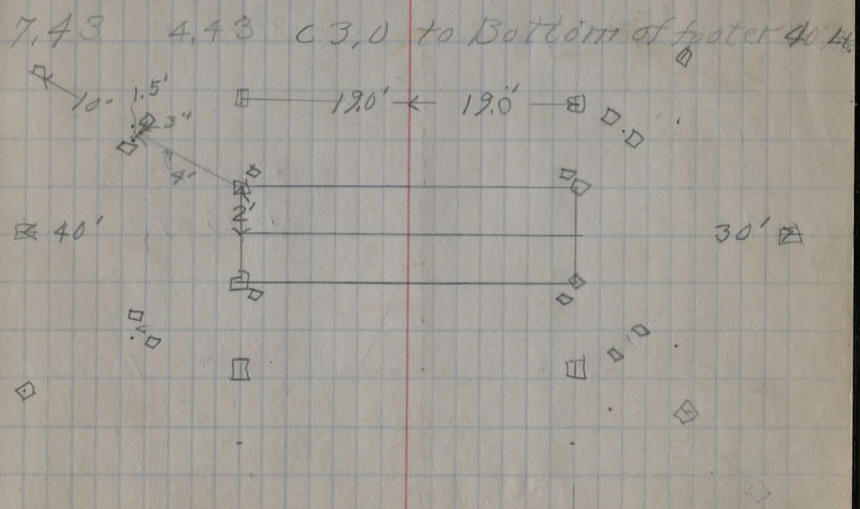
34+00 resetting stake 40' Lt
 stake 30' Rt
 2.43 C 5.0

April, 9 1931 49
 D. Parks
 T. Snyder clear 650
 Bent spike & root 30" Maple 25' Rt. Stake 29+75



12.92 7.92 C 5.0 to Bottom of footer Stake 30' Ft.
 12.92 10.92 C 2.0 to Bottom of footer Stake 30' Lt

May 8, 1931 D. Parks, T. Snyder
 Fair 75°



B.M. 0.41 1203.09 1202.68

51+90

1192.14 10.95 7.95 C 3.0 stake 30' Rt

1190.90 12.19 9.19 C 3.0 stake 30' Rt,

B.M. 0.99 1080.80 1079.81

14+70

B.M.

1068.26 12.54 12.04 C 0.5 stake 30' Rt,

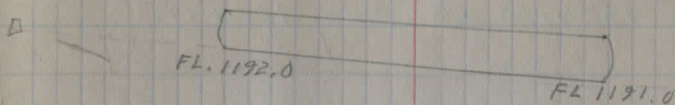
1069.27 11.53 6.58 C 5.0 stake 30' Lt,

April 20, 1931

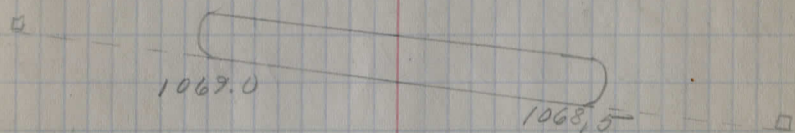
50

D. Parks
T. Snyder
Cloudy 80°

N. root 30" Locust 27' Rt, sta. 51+00



Bent spike N. side 15' Walnut 25' Rt. 20+15



April 20, 1931

51

D. Parks

T. Snyder

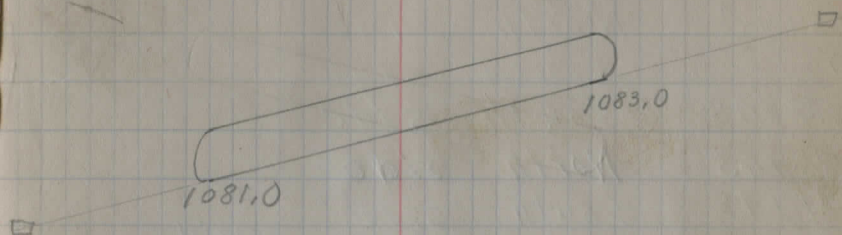
Cloudy 80°

30+35

B.M. 6.95 1090.55

1083.60

Bent spike S. root 30" Maple 25' Lt. sta. 29+77



1083.94

6.61

1.11

C 5.5

stake 30' Rt

1080.41

10.14

13.14

F 3.0'

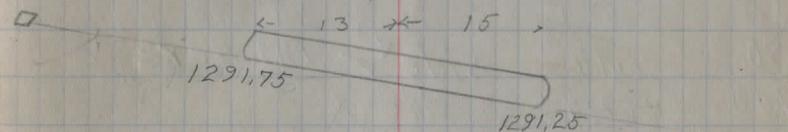
stake 30' Lt

69+80

B.M. 4.37 1299.22

1294.85

Two spikes N. root 24" Ash 27' Rt. sta. 66+98



1290.98

8.24

6.24

C 2.0

stake 30' Rt.

1292.06

7.14

3.86

C 3.5

stake 30' Lt.

April 21, 1931
D. Parks cloudy 70°
T. Snyder
Driveway Pipes

6+10	South side ✓	
13+90	North side ✓	
19+45	South side ✓	
24+05	South side ✓	
35+45	North side ✓	(m)
41+15	South side ✓	
49+45	South side	Deid. wanted
49+80	South side ✓	
49+90	North side ✓	
52+95	North side	
58+05	South side	
62+15	South side ✓	
72+05	South side ✓	
78+80	South side ✓	
81+70	North side ✓	
92+80	South side ✓	Roseum will place the
84+90	South side ✓	Not Needed Roseum
93+00	North side ✓	Put Here
102+80	South side ✓	not needed
107+05	South side ✓	
114+40	North side ✓	

107+05 S.

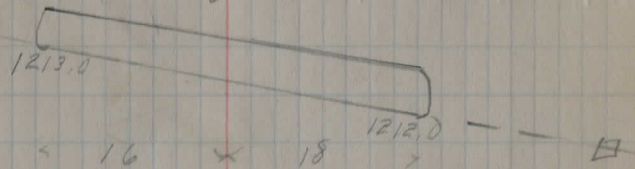
April 23, 1937
 D. Parks
 T. Snyder
 Cloudy 30'

90+85

B.M. 3.61 / 221.90

121829

N. root 24" evergreen 30' Rt, Sta. 91+25

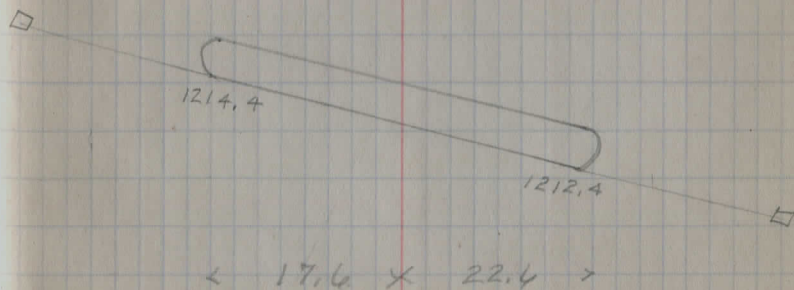


1211.65 10.25 5.76 C 4.5 stake 30' Rt

1213.41 8.49 4.99 C 3.5 stake 30' Lt

89+15

1221.90



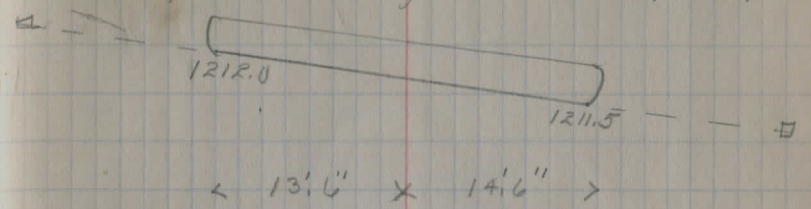
1212.02 9.88 10.88 F 1.0 stake 30' Rt

1215.03 6.87 3.37 C 3.5 stake 30' Lt

94+75

B.M., 1.93 1220.22 1218.29

N. root 24" evergreen 30' Rt, sta. 91+75



1211.22 9.00 6.50 C 2.5 stake 30' Rt.

1212.30 7.92 5.92 C 2.0 stake 30' Lt.

Check off Grades

Hub
Marked,
Rod
reading
on slope
Hub

Grade Rod

0+00	F0.1	12.00	11.9
1+00	C2.4	10.40	12.8
1+50			
2+00	C0.0	2.2	2.2
3+00	F2.6	8.2	5.6
4+00	C2.7	4.00	6.7
5+00	C5.1	2.9	8.0
6+00	F1.4	4.0	2.6
6+50	C3.1	3.8	6.9
7+00	F2.3	7.9	5.4
8+00	F1.5	5.1	3.6
8+40	F0.5	2.1	1.6
9+00	C2.7	5.5	8.2

May 5, 1931
D. Parks, T. Snyder
Cloudy 80°
N. side

55

S. side

F0.1	Berm	9.0 from E	.6 High	1.0 High	.4 High	9.0 from E	Berm
C2.4	Berm	11.0 from E	1.2 High	.9 High	.4 High	11.0 from E	Berm
							no ditch on S. side
C0.0	Ditch	11.5 from E	.6 Low	.3 Low	.5 low		no ditch on S. side
F2.6	Ditch	13.0 from E	.8 low	.4 low	.9 low		no ditch
C2.7	Ditch	13.0 from E	.9 low	.4 Low	.1 low	10.5 from E	Berm Ditch
C5.1	Ditch	10.0 from E	.5 Low	.2 Low	.3 Low	8.0 from E	Berm Ditch
F1.4	Ditch	13.0 from E	.25 from E	.8 Low	.2 Low		Berm & Ditch O.K.
C3.1	Berm	Ditch	.6 O.K.	.2 Low	.1 Low	.6 Low	Berm & Ditch O.K.
F2.3	Ditch	3.0 from E	10.0 from E	.9 Low	.1 Low	.3 Low	Berm O.K.
F1.5	Berm	8.5 from E	.2 High	.8 High	.7 High	12.0 from E	Berm Ditch
F0.5	Ditch	13.0 from E	.90 from E	.2 Low	.5 High		Grade Berm & Ditch O.K.
C2.7	Ditch	13.0 from E	10.0 from E	.6 High	.1 High	.7 High	Berm Ditch

9+45	C.05	5.4	5.9
10+00	F0.5	4.7	4.2
10+50	C2.0	4.2	4.2
11+00	C0.1	8.7	8.8
12+00	F0.4	3.3	2.9
12+50	0.0	4.3	4.3
13+00	F0.3	5.9	5.6
14+00	C0.6	4.3	4.9
15+00	C1.6	6.6	8.2
16	F3.9	10.3	6.4
17	C0.5	2.8	3.3
18	C0.9	0.9	1.8
19	C0.3	0.8	1.1

Ditch	Berm	Berm	Ditch
13.5 from E	10.5 from E	2 High, 8 High, 6 High	11.0 from E 14.0 from E
Berm & Ditch	O.K.	.6 Low .1 High .2 Low	Berm Ditch O.K. not well cut
Berm	Ditch	O.K.	.2 Low .1 High .1 Low
Berm	Ditch	10.0 from E	12.0 from E
Ditch	Berm	O.K.	13.5 from E
O.K.	13.5 from E	.3 Low .1 High .2 Low	Berm Ditch 10.0 from E 13.0 from E
Ditch	Berm	3.5 from E 8.5 from E	.1 High 3 High .1 Low
10.5 from E	Ditch	Berm	170
13.0 from E	9.0 from E	.Grade	Grade
Grade	Grade	Grade	O.K.
Ditch	Berm	13.0 from E 8.0 from E	.3 High 3 High .1 High
Berm	Berm	O.K.	O.K.
Ditch	Berm	13.5 from E 10.5 from E	Grade .1 High .2 Low
Berm	Berm	10.0 from E	
Ditch	Berm	13.0 from E 9.0 from E	.2 High 3 High .1 Low
Berm	Berm	O.K.	O.K.
Berm	Berm	O.K.	.5 Low .2 High .3 High
Berm	Ditch	10.0 from E	14.0 from E
Ditch	Berm	13.5 from E 10.0 from E	.2 Low .1 Low .2 Low
Berm	Ditch	O.K.	14.5 from E
Ditch	Berm	13.5 from E 14.5 from E	Grade Grade
Berm	Ditch	.3 Low	10.5 from E 13.5 from E
Ditch	Berm	13.0 from E 10.0 from E	.2 High 4 High .2 High
Berm	Berm	10.5 from E	

20	C1.1	10.8	11.9
21	C1.7	4.4	6.1
22	C1.0	7.5	8.5
23	C0.5	4.8	5.3
23+65	C2.0	2.4	4.4
24	C3.0	2.4	5.4
25	F0.3	4.9	4.6
26	F1.8	8.8	7.0

Sta. 27+00 to sta. 34+00 Grade not ready for a check Berms not made; No ditch line on S. side

Berm	10.0 front	.2 High	.6 High	.2 High	10.0 front	13.0 front			
Berm	Ditch	0, K	Grade	.3 High	.1 Low	9.0 front	13.0 front		
Ditch	Berm	13.1 front	11.0 front	.4 Low	.1 High	Grade	10.5 front	13.0 front	
Ditch	Berm	13.55 front	10.0 front	.1 Low	.2 High	.1 Low	10.0 front	13.0 front	
Ditch	Berm	0, K	10.0 front	.5 Low	.3 Low	.4 Low	Berm	Ditch	0, K
Ditch	Berm	13.5 front	10.5 front	.1 Low	.1 High	.1 Low	Berm	Ditch	0, K
Ditch	Berm	15 front	11.0 front	.4 Low	.7 High	.4 High	Berm	Ditch	0, K
Ditch	Berm	12.5 front	10.0 front	.6 Low	.4 Low	.6 Low			

SPECIAL ITEMS,

June 4, 1931. W.C. Marks + O.C. Scott. 58

41+00 36 lin. ft. 4" Drain Tile,

Outlets of Drains from \pm to both Side Ditches

97+90 to 99+30 140 lin. ft. 4" Drain Tile

in North Side Ditch.

97+80 to 99+40 160 lin. ft. 4" " "

" South " "

117+25 24 lin. ft. 15" corr. Iron Pipe
5 1/2 lin. ft. 12" Sec. Cast Iron Pipe

} 29' ^{Extra} Culvert across Mulberry Road
on W. Side of N. + S. Road.

79+00 36 lin. ft. 15" Corr. Iron Pipe,

Extra Culvert across Road.

34+00 Deduct 4.1 cu. yds. 1:8 Concrete
Add 6.0 " " 1:6 1/2 "

from Quantity shown on Plan.
to " " " "

37 C2.9 4.0 6.9

38 C2.1 3.7 8.1

Berri Ditch } 0.11, 5 High 1. High 4 High } Berri Ditch } 0.11

Survey of Mulberry Rd from
Heath Rd to Fawlers Mills Rd

A Temple
H. Patterson
D. Canfield

Sept. 55

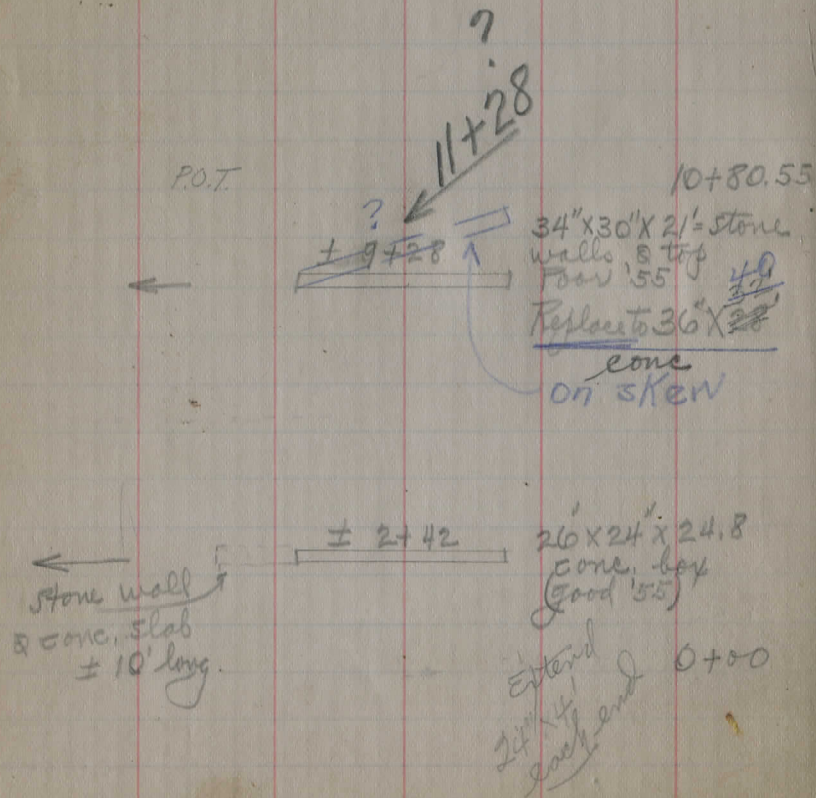
PT = 26+15.0

P.I. = 24+79.7

P.C. = 23+37.0

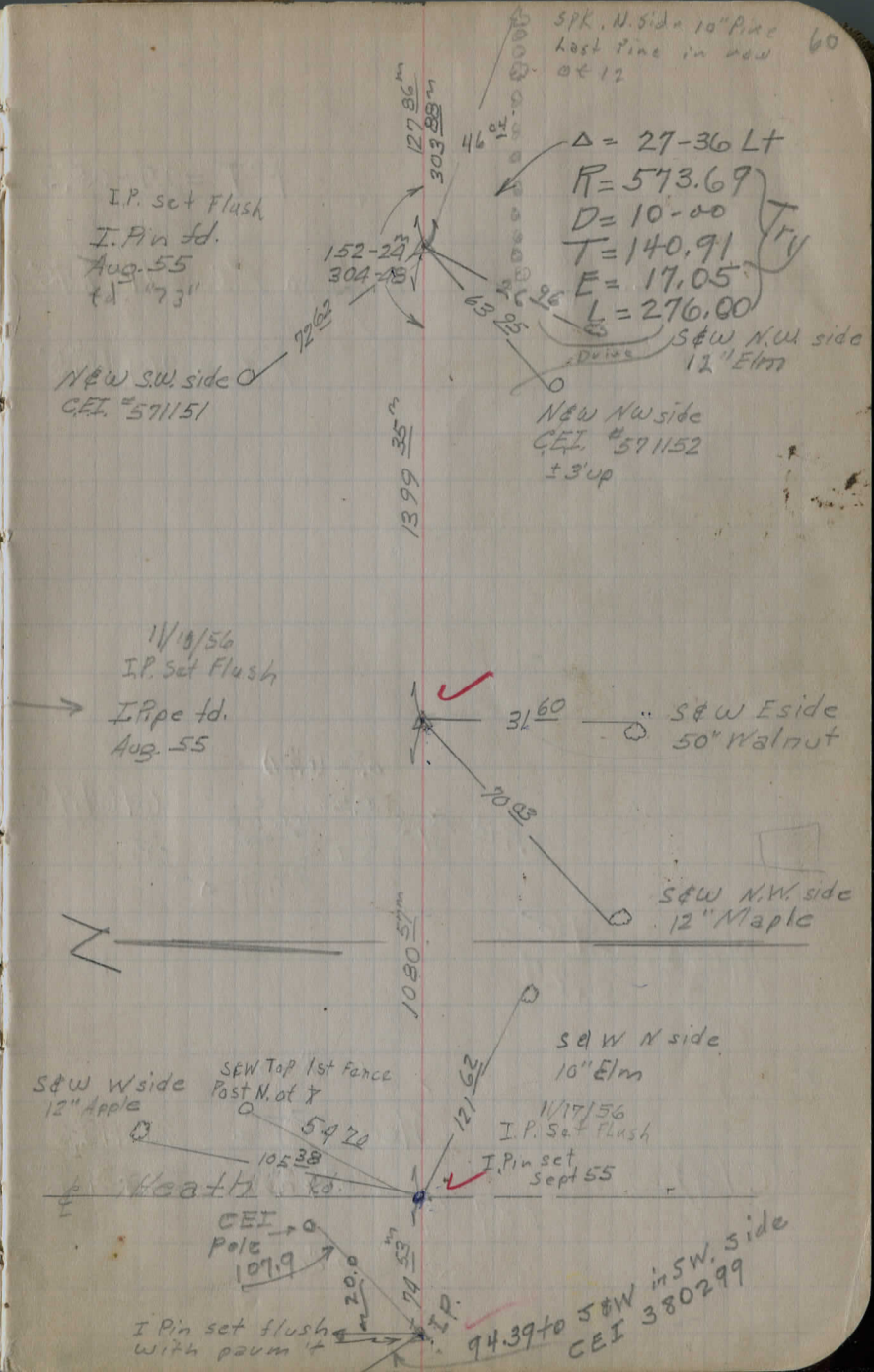
P.I.

P.O.T.



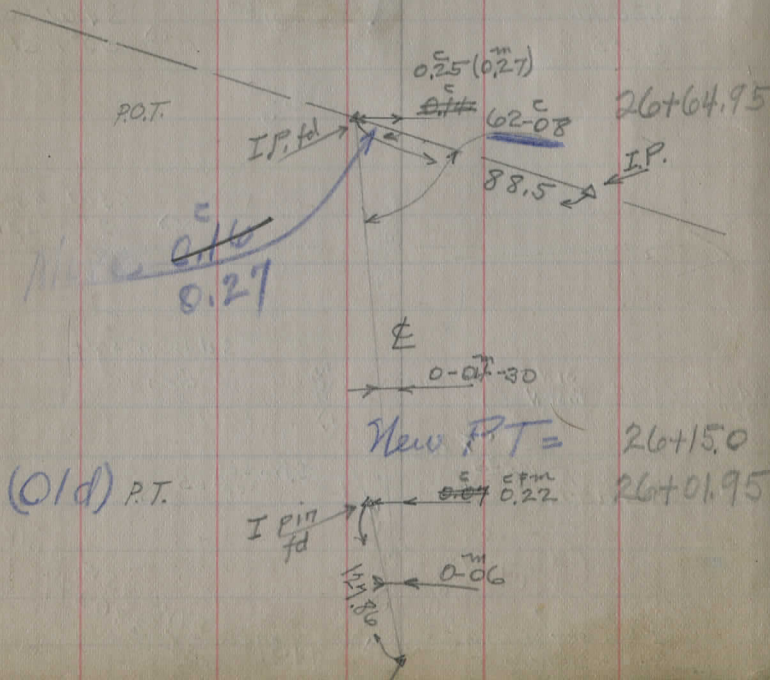
I.P. set Flash
I. Pin set
Aug. 55
td "73"

N&W SW side
CEI #571151

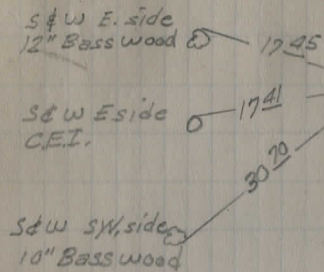


P.I.

PT = 29+05.5
 Δ 154.00 P.I. = 27+77.95
 PC = 26+45.5

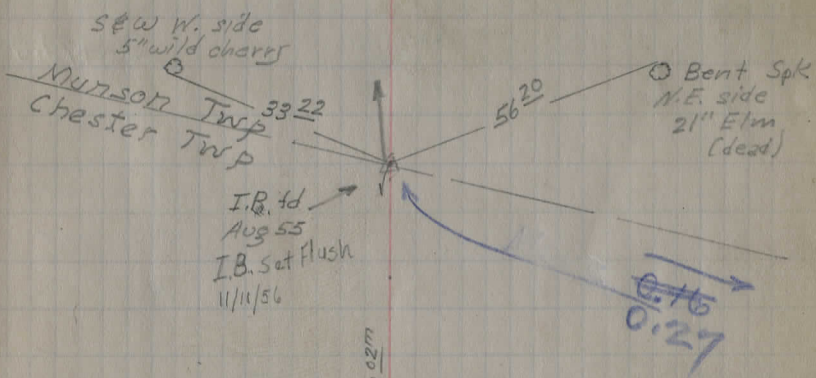


26-02 Rt



Δ = 26-00 Rt
 R = 573.69
 D = 10-00
 T = 132.45
 E = 16.06
 L = 260.00

I. Pin fd. & reset
 Aug. 55
 Raised to 4"
 11/10/56

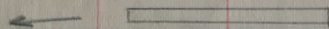


I.P. set flush
 11/10/56
 I. Pin fd
 Aug 55

0-28.70
 N&W W. side
 C.E.I. = 57/153
 ±2' up

Mulberry Trd (Munson) 1955

50+13.25



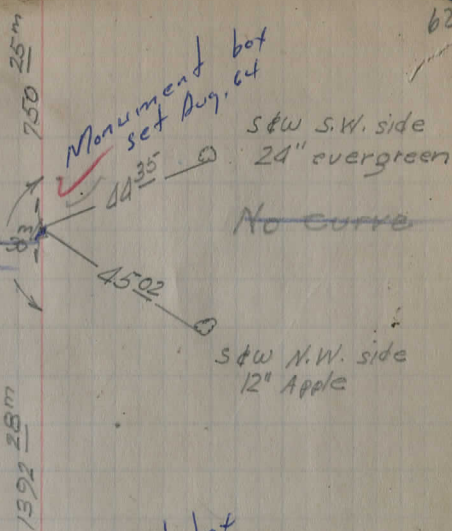
41+35
15" X 34.5 conc. pipe
found.

36+21.0

31+77.85

11/156
IP set flush
I bolt fd = P.O.T.
Aug 55

179-57-30
359-59



s&w E side
CEI # 571159

32 22

Monument bot set Aug. 64
IP set flush
11/156
spk set R.O.T.
Sept 55

P.O.T. =
0.21 5th
of spk

s&w w side
6" twin Basswood

60 01

443 15m

s&w N. side
20" Maple

11/156
IP set flush
spk set
Sept 55

P.O.T. =
0.25 5th
of spk

74 17
179-57-30
359-55

Monument bot set Aug 64

No curve

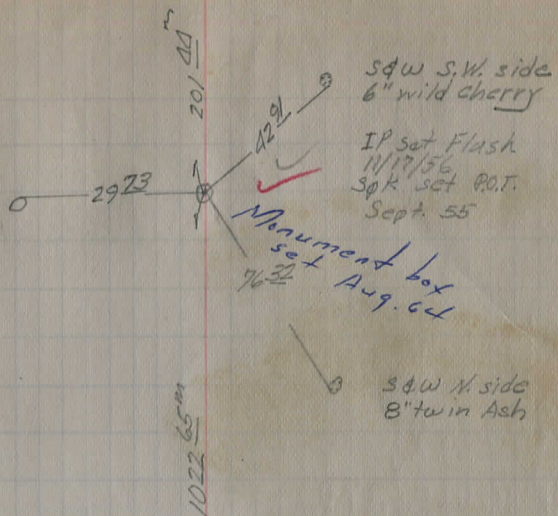
s&w s.w side
CEI # 571156

407 15m

s&w N. side
20" Walnut

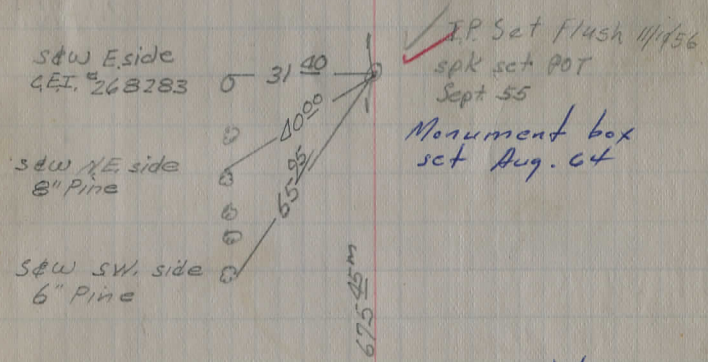
74+61.0

s.w. E side
C.E.I. #268290



64+38.95

s.w. E side
C.E.I. #268283

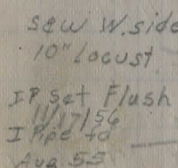


60+65

OK

← 48" x 54" x 37.8 cone box

s.w. W. side
10" Locust



P.T. 58+01.5

P.I. 57+63.50

P.C. 57+25.5

← 57+00 15" x 37.6 Corr. 57+00

Replace - 15" x 40 cone

C.E.I. # 571171 s.w. side
6" Basswood

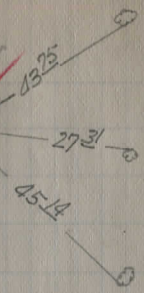
Monument box set Aug. 64

$\Delta = 3-48$ LT
 $R = 1146.28$
 $D = 5-00$
 $T = 38.02$
 $E = 0.63$
 $L = 76100$

90+90.2

I.P. set Flush
11/10/56
Monument box
set Aug 64

772 49m



613 28m

s&w N.W. side
of the S.W. stem
of cherry dump

6650

84+46.2

s&w E. side
8" cherry

3708

s&w N.E. side
8" stem of
triple locust
s&w set P.O.T.
I.P. set Flush
11/10/56

3612

783 15m

s&w N. side
20" cherry

6028

24" x 49' corr. pool → 78+55
Replace 24" x 52' cone.

P.I. 76+63.05

s&w set
Sept. 55
I.P. set Flush
11/10/56

179-37
357-02

Monument
set Aug 64

3543



Kotrlik
Barn

No. Curve

Mulberry Rd (1955) 121+40 =

$\Delta = 8-10 R$
 $\#R = 1432.69$
 $D = 4-00$
 $T = 100.19$
 $E = 3.50$
 $L = 200.00$

PT = 121+02.6
 PI = 120+
 PG = 119+02.6

119+50 =

24" X 40' Corr → 115+80 -

Replace 24" X 40' Cone

✓
 P.I. 107+62.75
 → I 105+60

15" X 38' cone open

Replace to 15" X 40' cone

Note: all angle points from here to Fowler's Mills Rd were set per this

Fbs 6-9

98+62.7

96+45

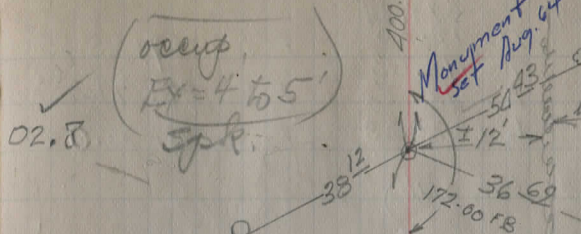
15" X 28' cone

(partly filled)

Replace 15" X 32' cone

15" X 28' cone
 Replace to 15" X 32' cone

02.8



S&W S.W. side
 CEF. house pole

15" X 32' cone
 Replace to 15" X 36' cone
 N. end filled

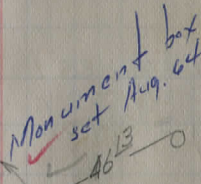
1240.07 FB

S&W S.W. side
 5" locust
 brush hedge front
 of Luckay
 Yard.
 (Spk set
 Sept 55)
 I.P. set flush
 11/2/56
 S&W S.E. side
 C.E.I. #190015

S&W SE. side
 24" Maple

Hartman
 house

S&W W. side
 30" Maple



S&W N.E. side
 C.E.I. #57899A

No curve

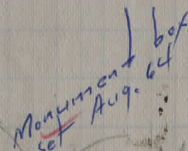
I.P. fd
 Aug 55
 I.P. set flush
 11/2/56

Spk ± 3' up
 24" elm

95.50

I.P. fd
 Aug. 55

I.P. set flush
 11/13/56



No curve

S&W S.E. side
 C.E.I.

$\Delta = 26-30 L$
 $R = 478.34$
 $D = 12-00$
 $T = 112.03$
 $E = 13.08$
 $L = 220.83$

$PT = 137+25.85$
 $PI = 136+17.65$
 $PC = 135+05.0$

6.67 = Top of footer to bot. slab
 10.5 = Clear span
 34.0 = Over all length
 (Includes
 6.5 ext. S. end & 3 ft. N. end)

Bridge 130 ± 50

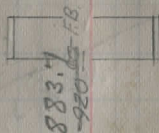
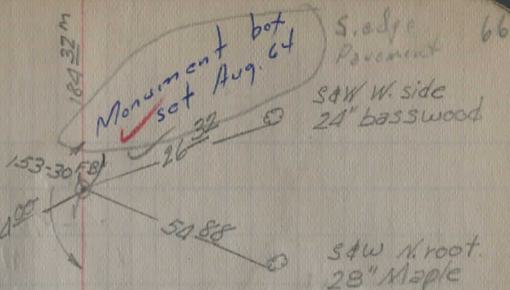
$\Delta = 21-35 L$
 $R = 7-00$
 $E R = 817.02$
 $T = 156.0$
 $E = 14.17$
 $L = 308.3$

$PT = 128+89.95$
 $PI = 127+37.65$
 $PC = 125+81.65$

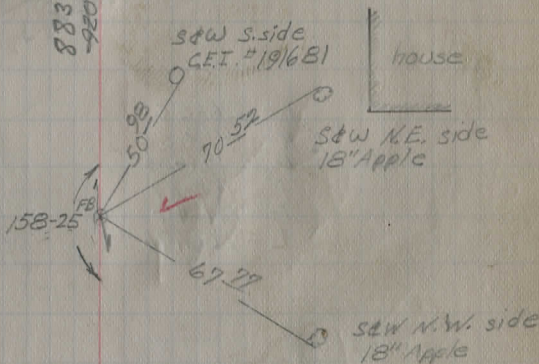
124+02.0

occult.
 $EC = \pm 12'$

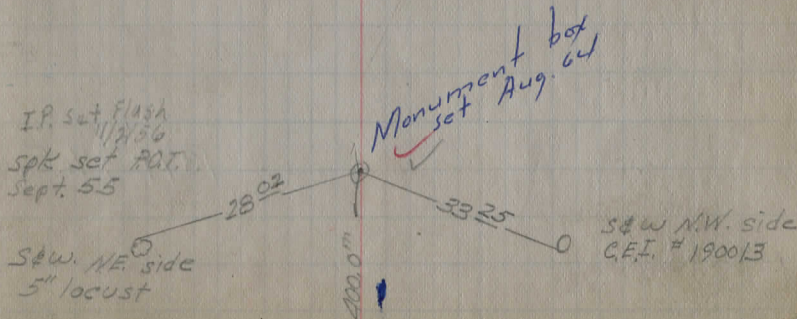
Spk. set
 Sept. 55
 I.P. set Flash
 11/2/56
 S&W S.W. side
 24" Maple



occult.
 $EC = 15' \pm$
 Spk. set
 Sept 55
 I.P. set
 11/10/56



I.P. set Flash
 11/2/56
 Spk. set PAT.
 Sept. 55

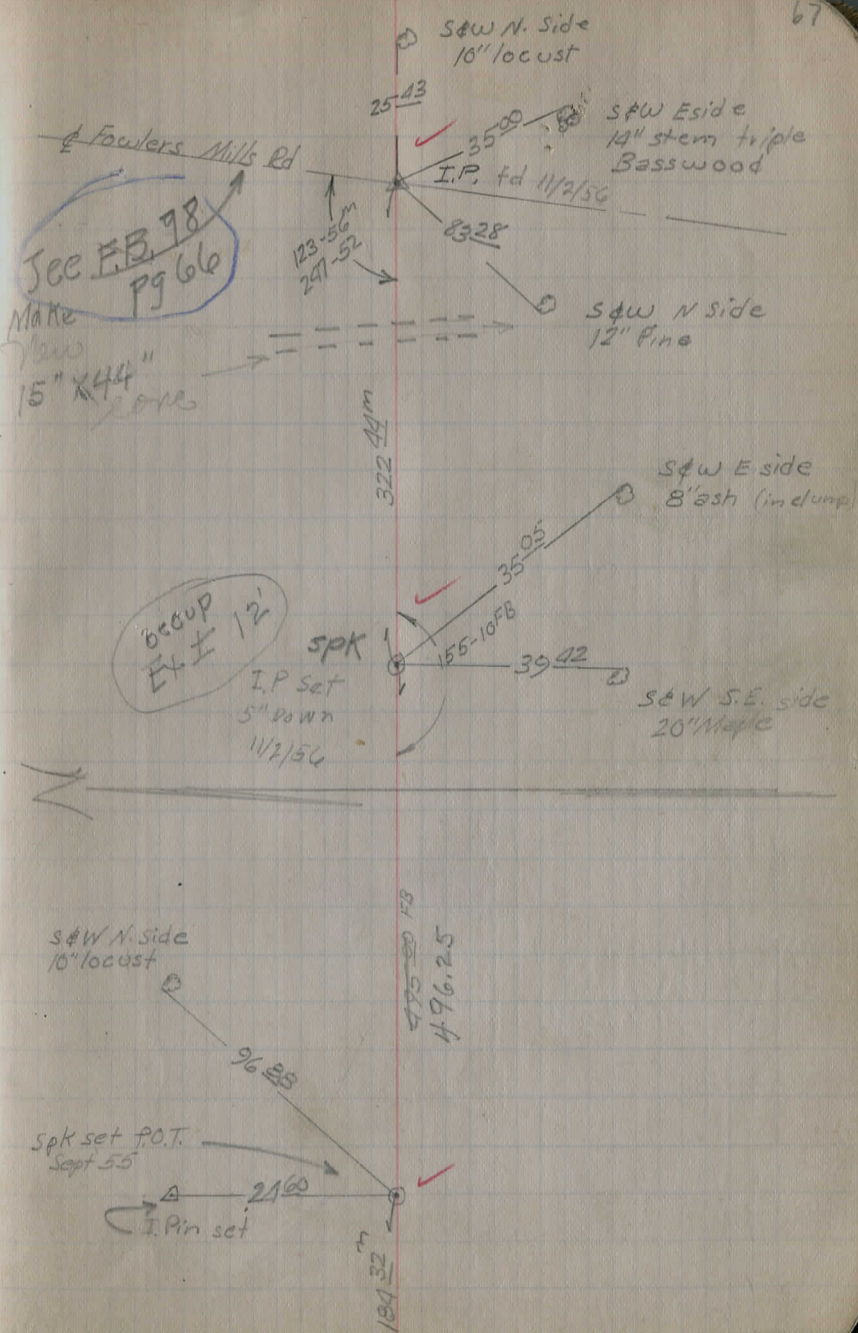


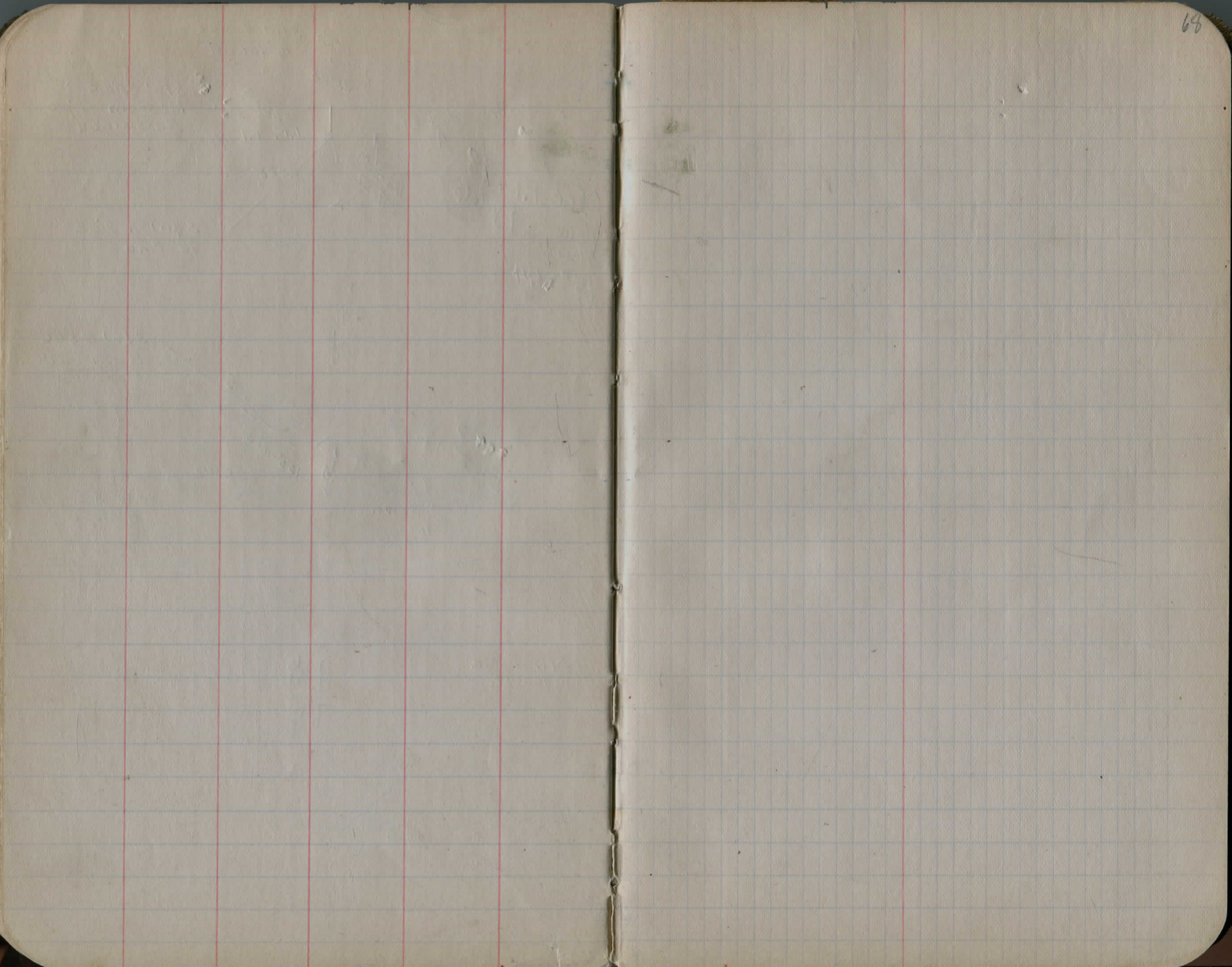
= PI. 144 + 28.25
 = 42 + 82.35 Fowler's
 Mills Rd Notes
 FB 98 p 66

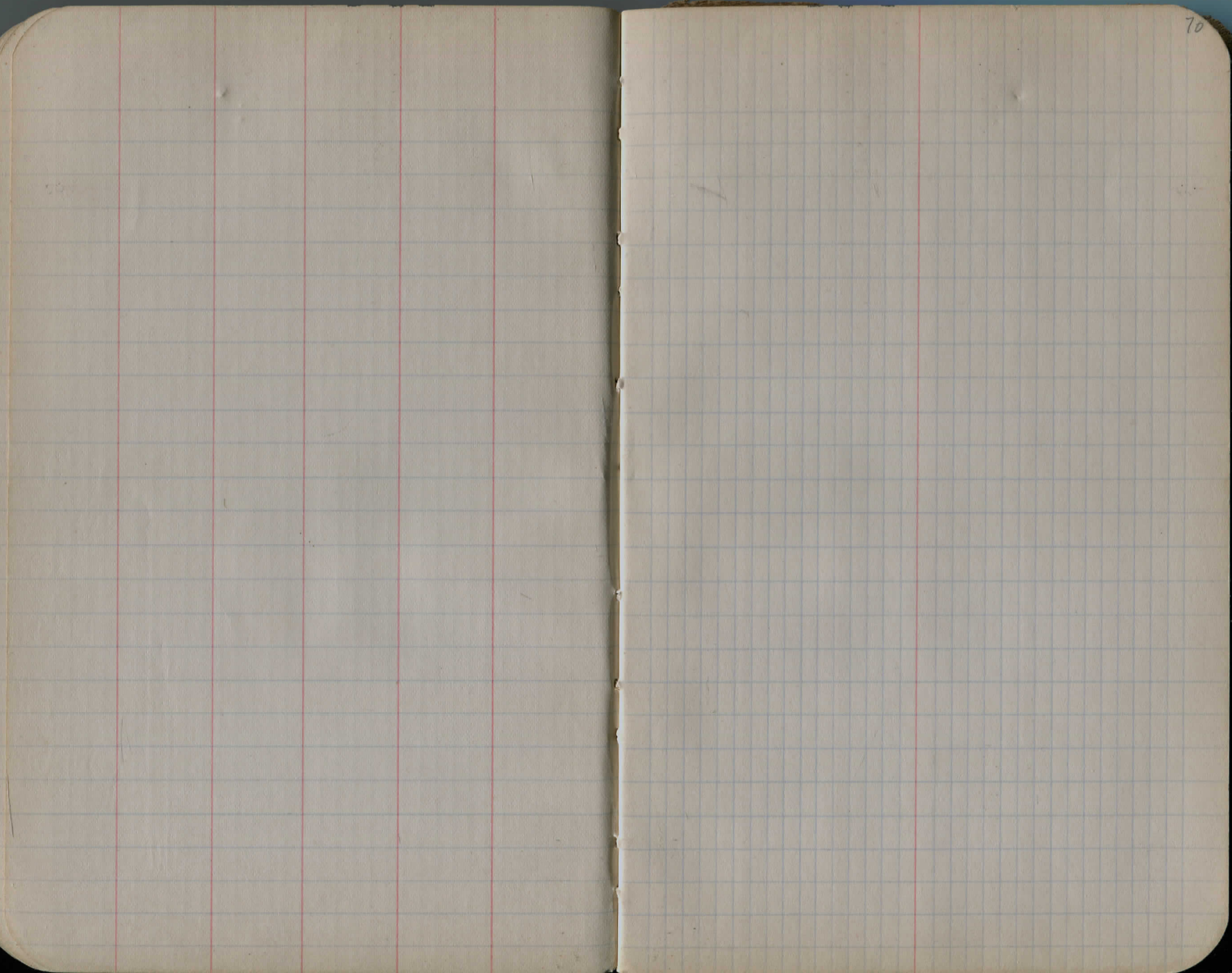
$\Delta = 24.50$
 $R = 478.34$
 $D = 12.00$
 $T = 105.32$
 $E = 11.46$
 $L = 206.94$

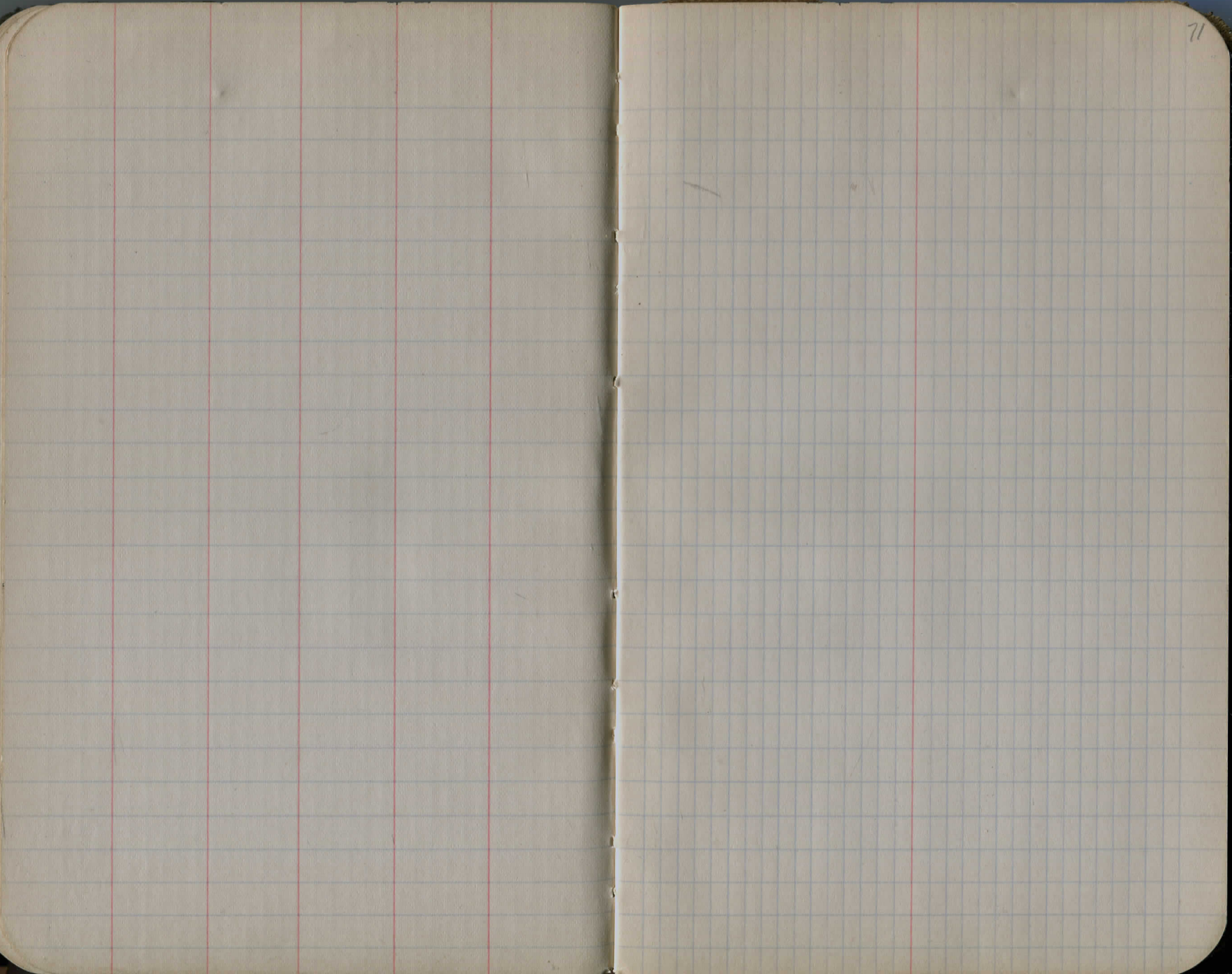
PT. 142 + 11.1
 PI = 141 + 09.45
 PC = 140 + 04.15

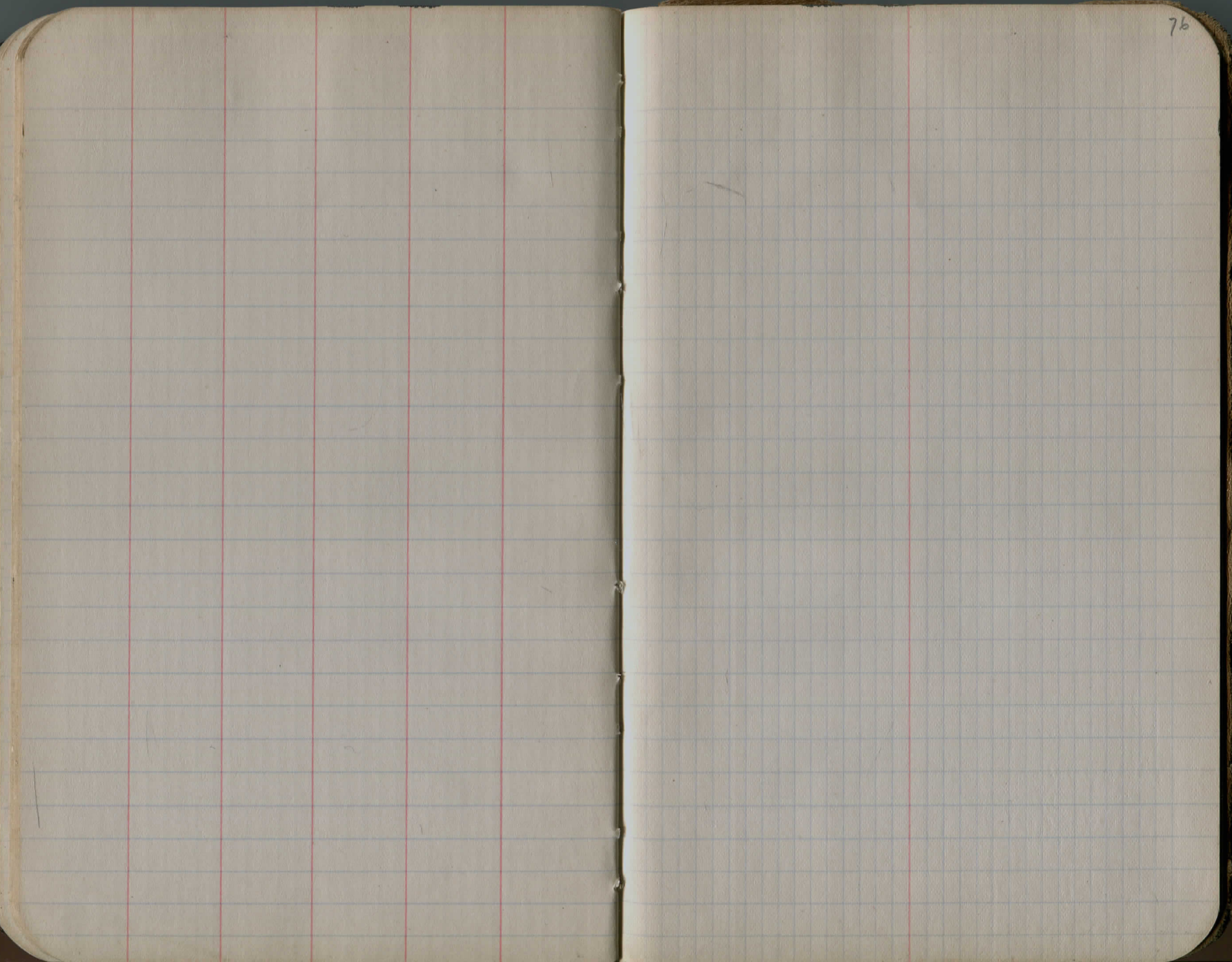
137 + 97.5

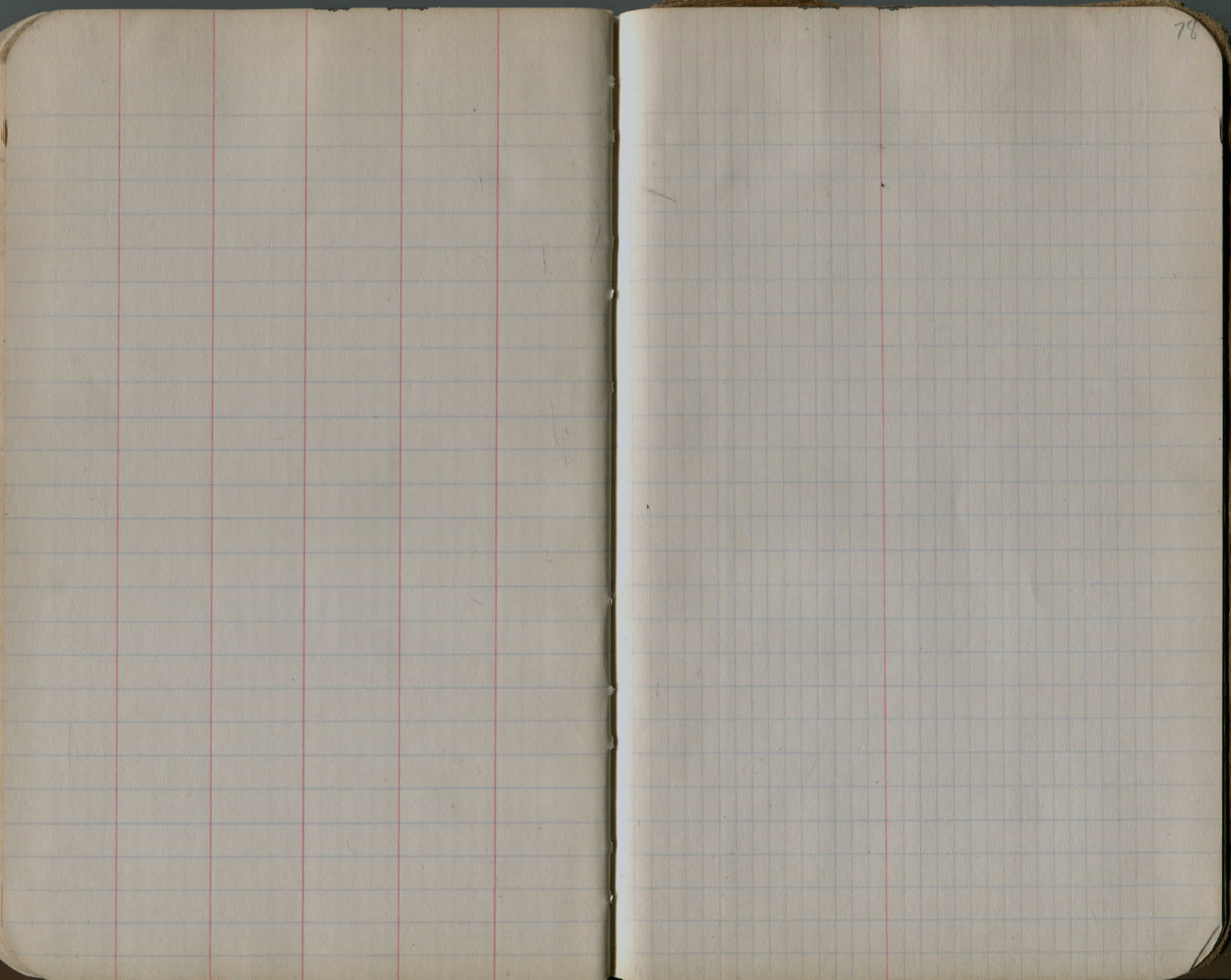


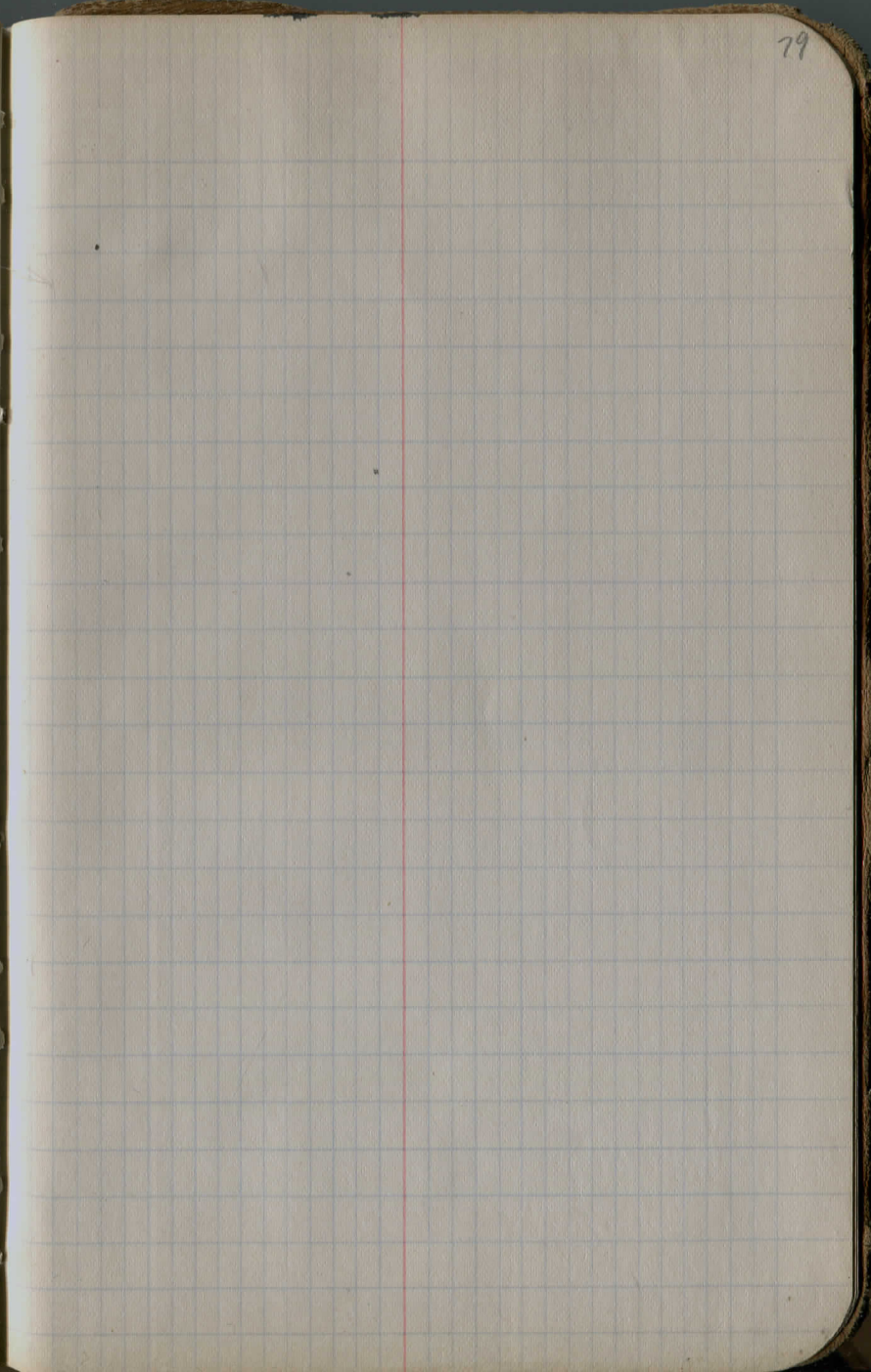
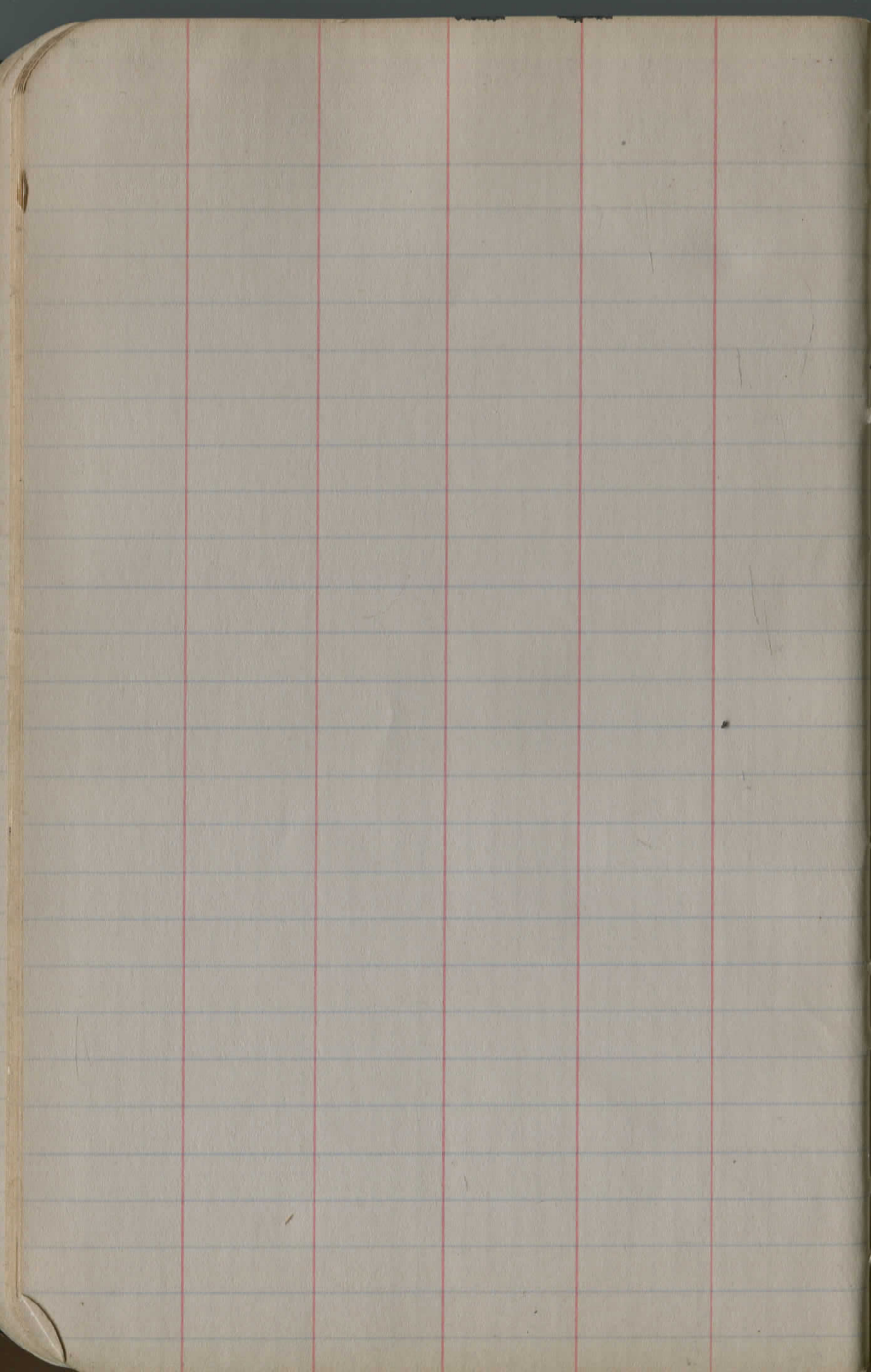


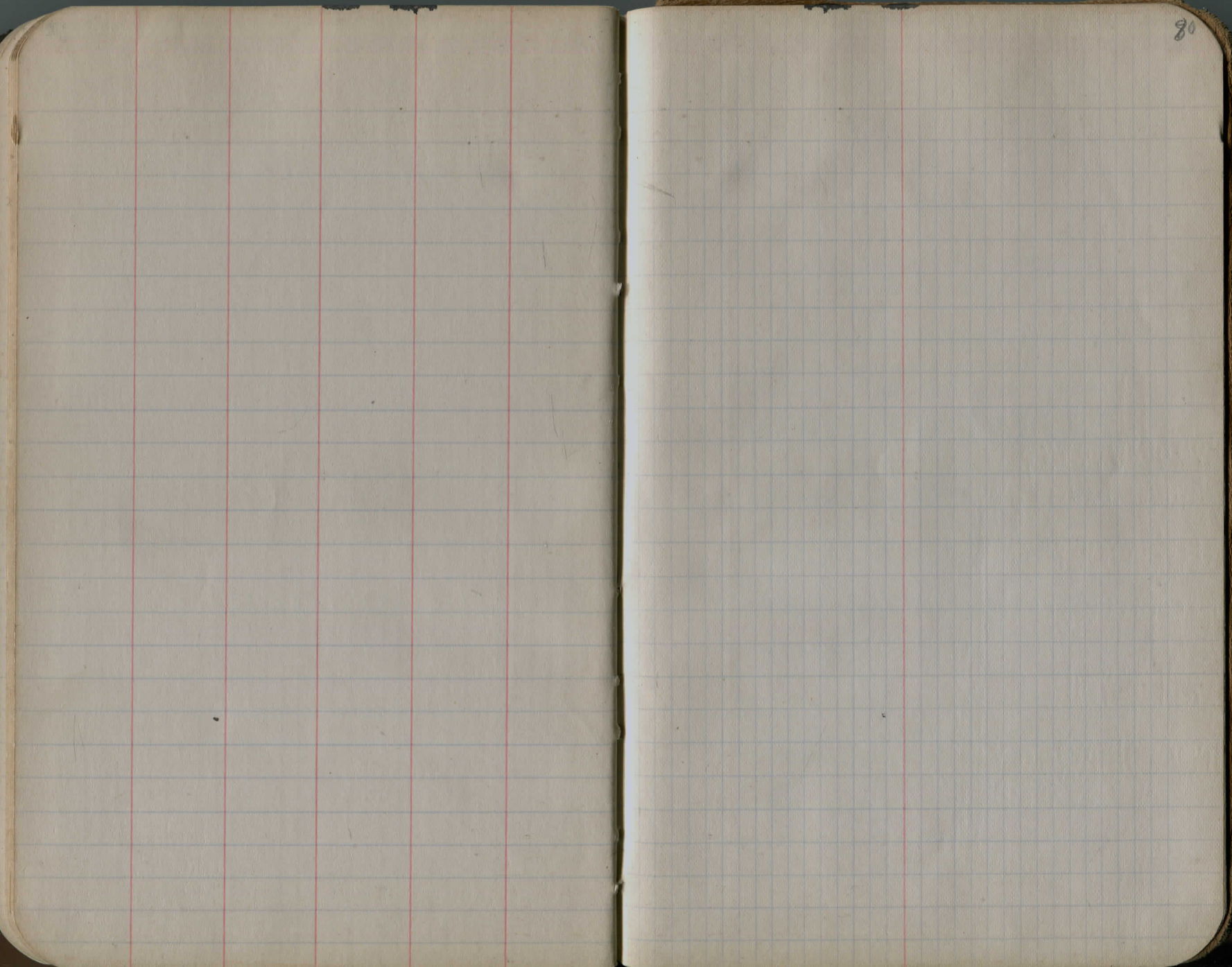












DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder
stake for any width roadway, slope 1 1/2 to 1.
If ground is nearly level, the cut or fill at side
stake is located by the double entry method in
left column and top row. The number in body

from side stake to slope stake. If ground is not

IMPROVED TABLES

AND

INFORMATION

To find Tangent and External for curve of
any other degree, divide by degree of curve and
add connection found in column of connections.
Degree of curve with a given L may be found
by dividing tangent (or external), opposite L by
given tangent (or external).

The distance from a point on the tangent to
the curve is very nearly the square of the tangent
length divided by twice the radius.

X-section + Topo

Mulberry Rd North side
#39 Pt Sec B

39+45 To 47+84

CHAPIN → EAST.

Mulberry Rd X-sections + Topo
North side

Assumed B.M. 100.00 & § chapin + Mulberry

sta. N.

41+50

41+49 30.2'

WIRE FENCE @

41+47 28.2'

C.F.I.

41+0

40+50

40+0

39+67 17'

End 24" Conc. Pipe

39+64

& chapin

39+50

39+45 17'

24" Conc. Pipe Crossing

B. Kosie
 D. Kosie
 P. Ranney
 9/25/67

46 + 62.35
 Mulberry + East Hill ①

North

$\frac{100.00}{6.20}$	$\frac{100.65}{5.55}$	$\frac{99.50}{6.70}$	$\frac{101.10}{5.10}$	$\frac{101.67}{4.53}$	101.83 4.37
30	20	17	13	9	

END GENCE 48 W.
 OF O.P.

$\frac{97.9}{6.79}$	$\frac{98.76}{5.54}$	$\frac{98.76}{7.14}$	$\frac{98.76}{5.29}$	$\frac{98.76}{6.10}$	101.22 4.98
30	22	18	14	9.4	

$\frac{98.35}{7.35}$	$\frac{98.35}{6.39}$	$\frac{98.35}{7.25}$	$\frac{98.35}{6.45}$	$\frac{98.35}{5.75}$	100.61 5.59
30	22	17	13	9.5	

$\frac{97.80}{7.80}$	$\frac{97.02}{7.45}$	$\frac{97.02}{9.18}$	$\frac{97.02}{6.59}$	$\frac{97.02}{6.29}$	100.17 6.03
30	24	17	12	9.5	

9.44

100.00
6.20

$\frac{6.81}{30}$	Rd.	$\frac{6.44}{9}$	99.89 6.31
-------------------	-----	------------------	---------------

Chapman St 9.34

H.I. 106.20

②

sta. N

44+0

43+90

29'

8" Locust

43+50

43+0

42+79

16.5

End 30" Conc. Pipe

42+61

✓

5' Dirt DR. ^{22' Above} 12' DR.

42+59

16.5

Begin 30" Conc. pipe

42+50

42+0

North

$$\begin{array}{r} 103.63 \\ 9.93 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 104.61 \\ 8.95 \\ \hline 24 \end{array}$$

$$\begin{array}{r} 102.26 \\ 11.33 \\ \hline 17 \end{array}$$

$$\begin{array}{r} 104.55 \\ 9.10 \\ \hline 12 \end{array}$$

$$\begin{array}{r} 105.06 \\ 8.50 \\ \hline 8 \end{array}$$

105.16
8.43

$$\begin{array}{r} 103.80 \\ 9.76 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 102.96 \\ 10.60 \\ \hline 20 \end{array}$$

$$\begin{array}{r} 101.59 \\ 12.00 \\ \hline 17 \end{array}$$

$$\begin{array}{r} 103.71 \\ 9.81 \\ \hline 12 \end{array}$$

$$\begin{array}{r} 104.15 \\ 9.41 \\ \hline 8 \end{array}$$

104.29
9.30

$$\begin{array}{r} 102.23 \\ 3.97 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 102.99 \\ 3.21 \\ \hline 24 \end{array}$$

$$\begin{array}{r} 100.10 \\ 5.50 \\ \hline 16.5 \end{array}$$

$$\begin{array}{r} 102.49 \\ 3.91 \\ \hline 13 \end{array}$$

$$\begin{array}{r} 103.33 \\ 2.87 \\ \hline 8.5 \end{array}$$

103.56
2.64

H.I. 113.59

G.09

Crossing DR. 5.89

$$\begin{array}{r} 101.95 \\ 1.25 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 102.55 \\ 3.65 \\ \hline 23 \end{array}$$

$$\begin{array}{r} 100.85 \\ 5.35 \\ \hline 17 \end{array}$$

$$\begin{array}{r} 102.40 \\ 3.80 \\ \hline 14 \end{array}$$

$$\begin{array}{r} 102.78 \\ 3.42 \\ \hline 8.4 \end{array}$$

102.83
3.37

$$\begin{array}{r} 100.20 \\ 5.5 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 101.80 \\ 4.80 \\ \hline 20 \end{array}$$

$$\begin{array}{r} 100.10 \\ 6.10 \\ \hline 17 \end{array}$$

$$\begin{array}{r} 101.10 \\ 5.10 \\ \hline 14 \end{array}$$

$$\begin{array}{r} 102.16 \\ 4.04 \\ \hline 8.7 \end{array}$$

102.31
3.89

H.I. 106.20

③

sta N

45+50

6:11

6:11

7' B.D.

108.00
5.50
30

45+0

6:11

6:11

6' B.D.

105.60
7.96
30

44+96.1

26.5

(3) 5" Locust

44+91

26.5

6" Locust

44+78

26'

12" Locust

44+74

29'

1" Tree

44+67

25'

8" Locust

44+60

29'

6" Tree

44+50

104.00
9.50
30

44+38

26'

6" Locust

44+33

26'

10" Locust

44+12

23'

6" Locust

$$\begin{array}{r} 108.26 \\ 5.70 \\ \hline 21 \end{array}$$

$$\begin{array}{r} 104.69 \\ 8.90 \\ \hline 20 \end{array}$$

$$\begin{array}{r} 105.09 \\ 8.17 \\ \hline 13 \end{array}$$

$$\begin{array}{r} 107.55 \\ 6.01 \\ \hline 12 \end{array}$$

$$\begin{array}{r} 108.23 \\ 5.33 \\ \hline 9 \end{array}$$

$$108.80$$

$$1.79$$

$$\begin{array}{r} 107.11 \\ 6.25 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 104.02 \\ 9.59 \\ \hline 20 \end{array}$$

$$\begin{array}{r} 103.89 \\ 9.70 \\ \hline 15 \end{array}$$

$$\begin{array}{r} 107.06 \\ 6.5 \\ \hline 11 \end{array}$$

$$\begin{array}{r} 107.39 \\ 6.17 \\ \hline 8.5 \end{array}$$

$$107.60$$

$$5.99$$

$$\begin{array}{r} 106.76 \\ 6.80 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 103.14 \\ 10.45 \\ \hline 20 \end{array}$$

$$\begin{array}{r} 103.41 \\ 10.15 \\ \hline 15 \end{array}$$

$$\begin{array}{r} 105.64 \\ 7.92 \\ \hline 12 \end{array}$$

$$\begin{array}{r} 106.21 \\ 7.35 \\ \hline 8 \end{array}$$

$$106.36$$

$$7.23$$

9' wide

④

sta. N.

47+84

End deep Ditch

47+50

2:1

2:1

1' B.D.

47+0

2:1

1:1

4' B.D.

468

4 E.P.

6" x 6" x 8.5'
BEGIN WOODEN G.R.

46+50

2:1

1:1

5' WIDE

427

4' E.P.

END WOODEN G.R. 6" x 6" x 8.5'

44+0

10:1

B.D. 6.5'

45+60

24'

12" Locust

45+57

Ditch Runs North

45+50

24'

6' Locust

$\frac{111.29}{2.30}$	$\frac{111.68}{1.91}$	$\frac{109.77}{3.20}$	$\frac{112.47}{1.10}$	$\frac{113.05}{0.54}$	113.04
$\frac{30}{22}$	$\frac{19}{16}$	$\frac{19}{16}$	$\frac{113.05}{9.7}$	0.55	

$\frac{110.19}{3.10}$	$\frac{111.13}{2.40}$	$\frac{108.87}{4.72}$	$\frac{111.79}{1.80}$	$\frac{112.61}{0.98}$	112.54
$\frac{30}{22}$	$\frac{19}{14}$	$\frac{19}{14}$	$\frac{112.61}{9.5}$	1.05	

Average

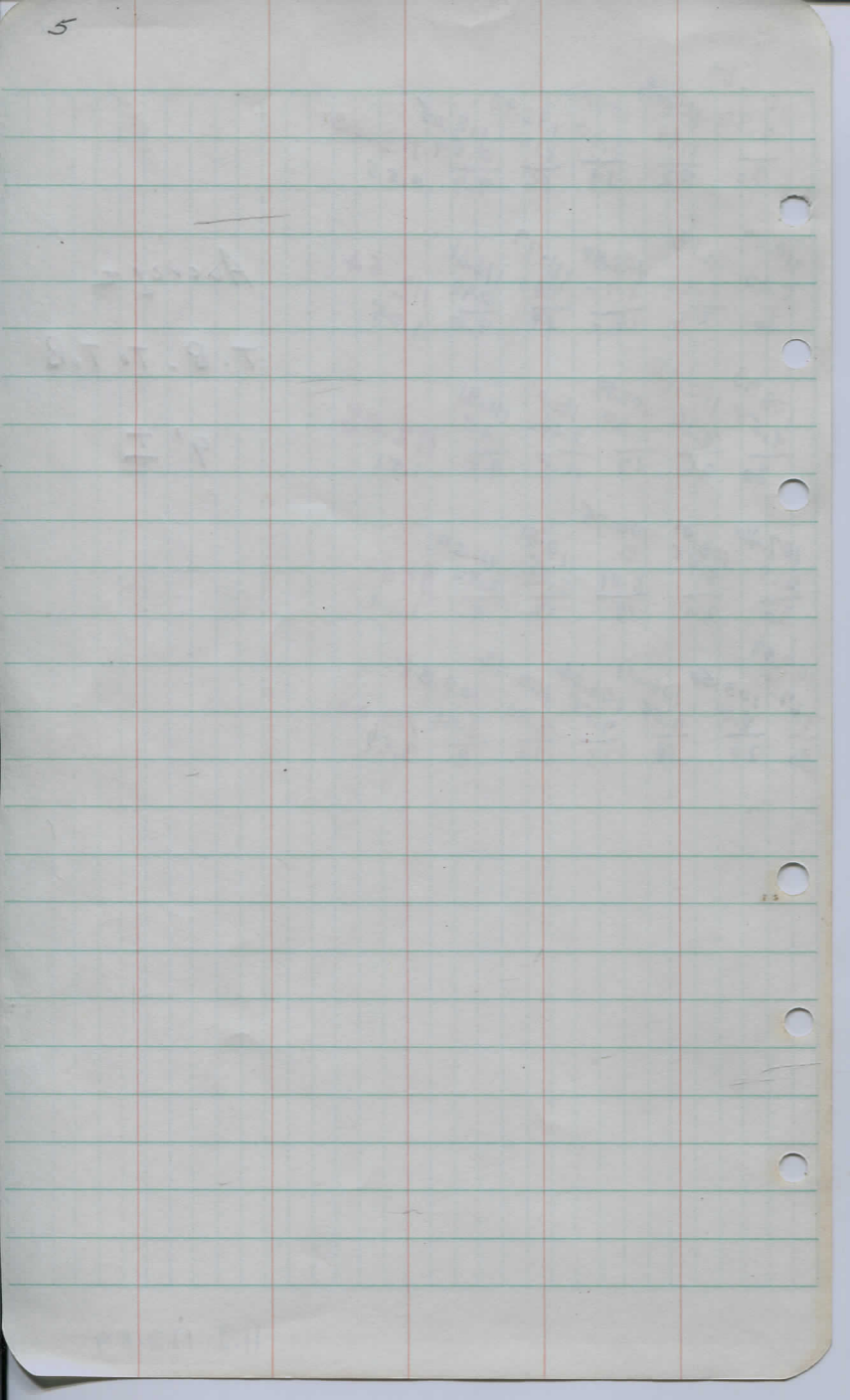
T.B. to T.B

$\frac{108.98}{4.58}$	$\frac{110.20}{3.36}$	$\frac{107.59}{6.00}$	$\frac{111.07}{2.47}$	$\frac{111.91}{1.45}$	112.08
$\frac{30}{21}$	$\frac{19}{17}$	$\frac{12.5}{9.5}$	$\frac{112.08}{1.51}$		

9' ±

$\frac{107.46}{6.10}$	$\frac{108.01}{5.55}$	$\frac{106.75}{0}$	$\frac{110.81}{2.75}$	$\frac{111.20}{2.30}$	111.30
$\frac{30}{20}$	$\frac{18}{12}$	$\frac{111.30}{2.29}$			

$\frac{107.89}{5.67}$	$\frac{108.50}{5.00}$	$\frac{106.01}{7.55}$	$\frac{106.04}{7.55}$	$\frac{109.12}{4.44}$	$\frac{109.84}{3.72}$	110.00
$\frac{30}{20}$	$\frac{18}{13}$	$\frac{110.00}{3.59}$				



♀ ♀ Mulberry + Chapin 5

Assumed B.M. 100.00

+ 6.20

H.I. 106.20

T.R. - 2.11

Elev 104.09

+ 9.50

H.I. 113.59

Reliance Universal Inc.



Concrete Products Division

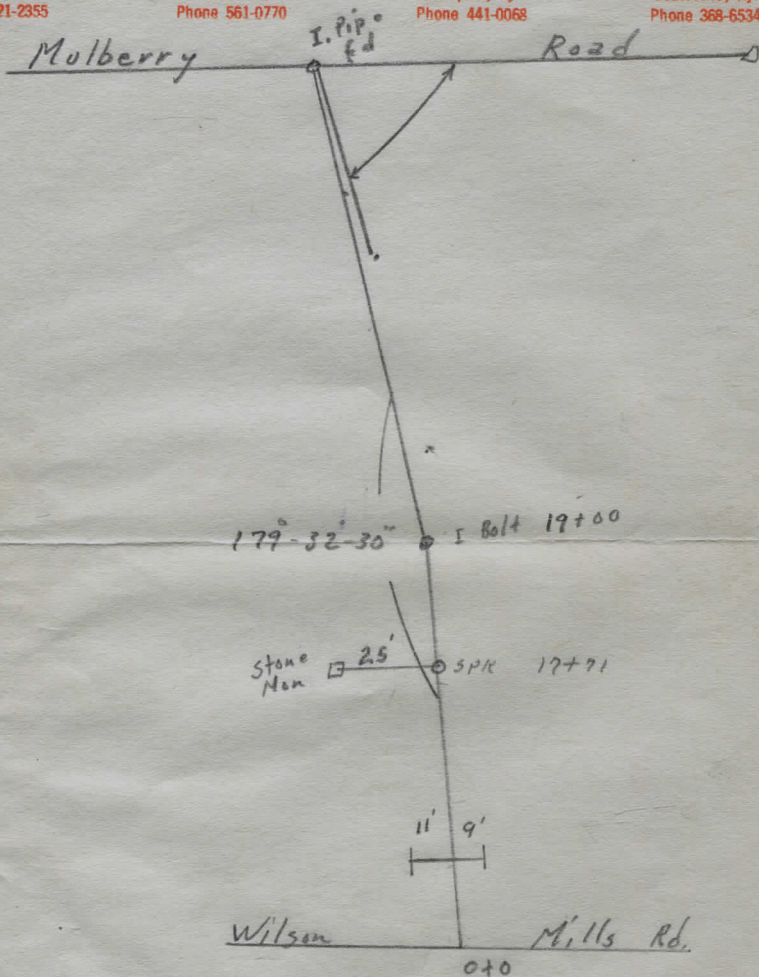
PLANTS AND OFFICES

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Reliance Universal Inc.



Concrete Products Division

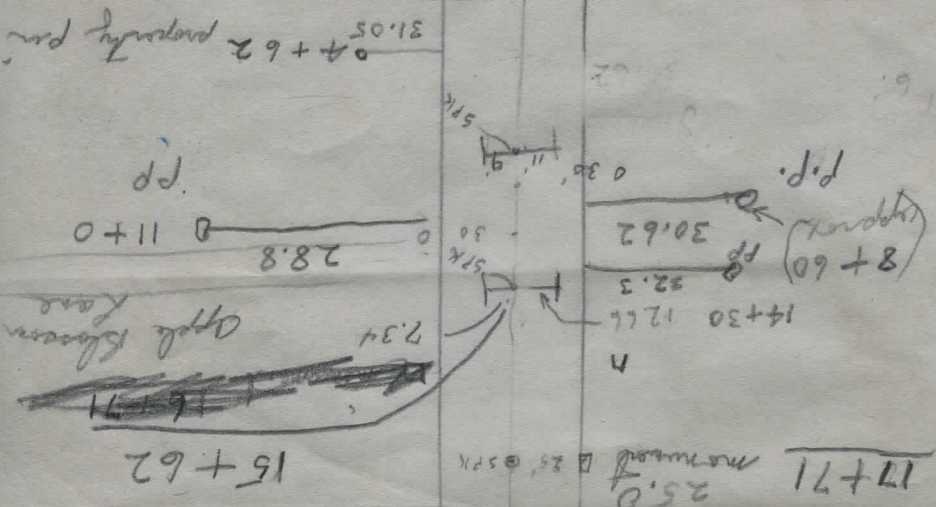
PLANTS AND OFFICES

COLUMBUS, OHIO
500 W. Whittier St.
Columbus 15, Ohio
Phone 221-2355

BRIDGEVILLE, PA.
Steen and Thom's Run Road
Pittsburgh 20, Pa.
Phone 561-0770

MELBOURNE, KY.
P.O. Box 10
Newport, Ky.
Phone 441-0058

LOUISVILLE, KY.
P.O. Box 13027 — Grade Lane
Louisville, Ky.
Phone 368-6534



**SEWER, CULVERT AND PRESSURE PIPE — LO-HED AND FLAT BASE PIPE
INNER CIRCLES TUNNELINER — PRECAST, PRESTRESSED BRIDGE SECTIONS
HI-HED PIPE — AMSEAL AND RUBBER GASKET JOINTS**

21°35'

60

7260

35

420

1295.0

1260.0

3508

3360

1400

5250

10560

53

1109

1087.8

1096.4

2 | 218.42

7 | 109.21

156.0

7 | 103.16

14.7

27.3

21

273

546

57.33

9°50'

10°47.33

50 0.3

48.25

66

47.59

175

16

109

95

53

25.5

40.5

50.33

PLEASE RETURN TO
GEAUGA COUNTY ENGINEER
COURT HOUSE
CHARDON, O.
PHONE 250-X

528 | 2728

2240

1384

1056

324

50

48.25

15.25

52.5

2.9

11.46

53 | 5700

400

